



Optimizing Stormwater Management to Protect Streams from Erosion



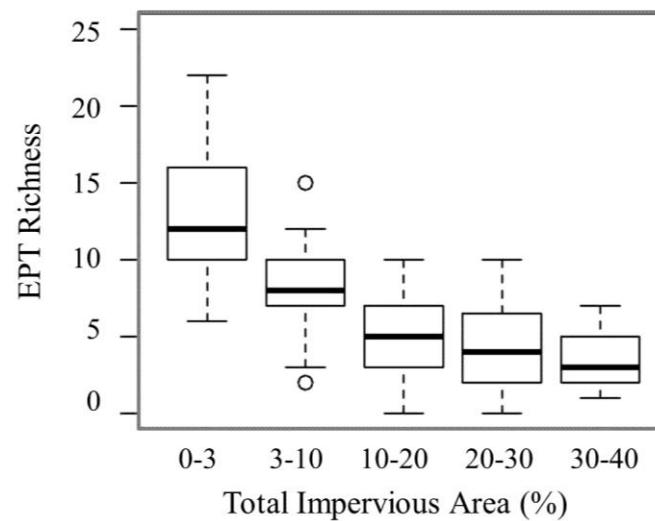
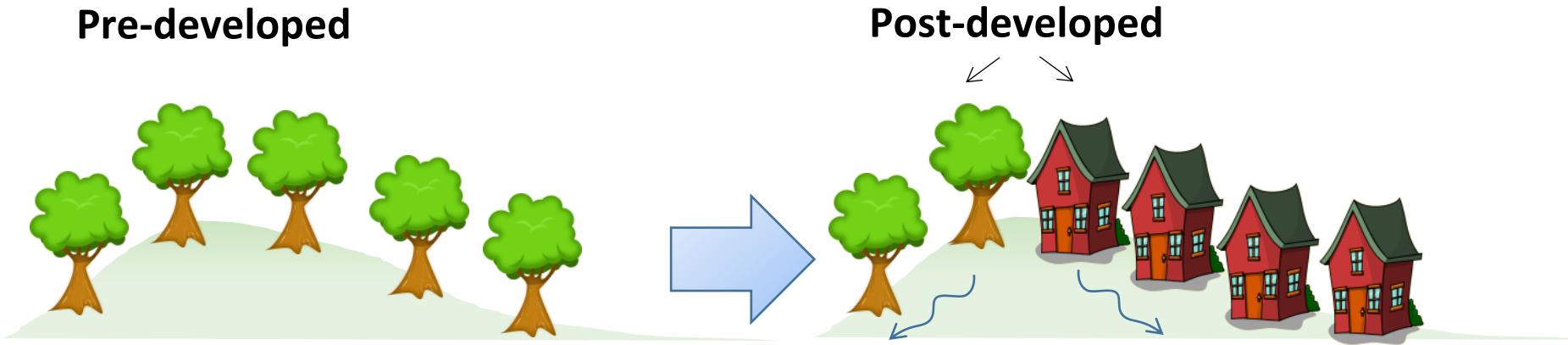
Dr. Bob Hawley, PE

Central Ohio SW & EC Expo, 2/26/16



Survey

How Many of You Work in Watersheds with Streams Impaired by Stormwater?



Adapted from Hawley et al.
(In revision, Freshwater Science)

The Urban Stream Syndrome

(Walsh et al., 2005; Booth, 2005, etc.)

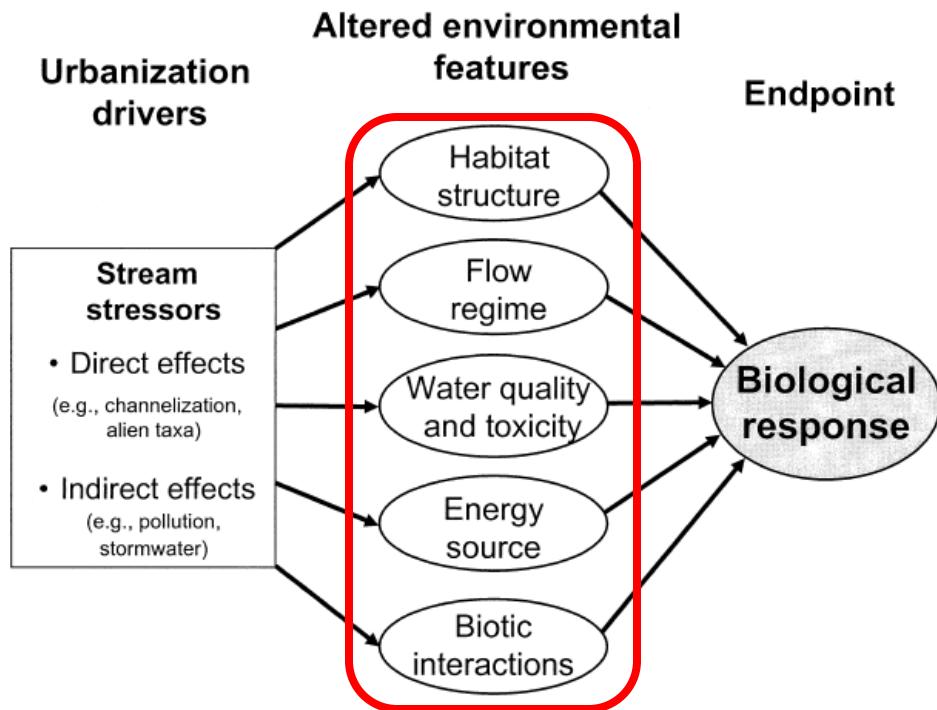


FIG. 1. Five environmental features that are affected by urban development and, in turn, affect biological conditions in urban streams (from Booth et al. 2004, reprinted with permission of the American Water Resources Association; modified from Karr 1991, Karr and Yoder 2004).



Stream Function Pyramid

(Adapted from Harmon et al., 2012)



Biological

Physicochemical

Geomorphology

Hydraulics

Hydrologic

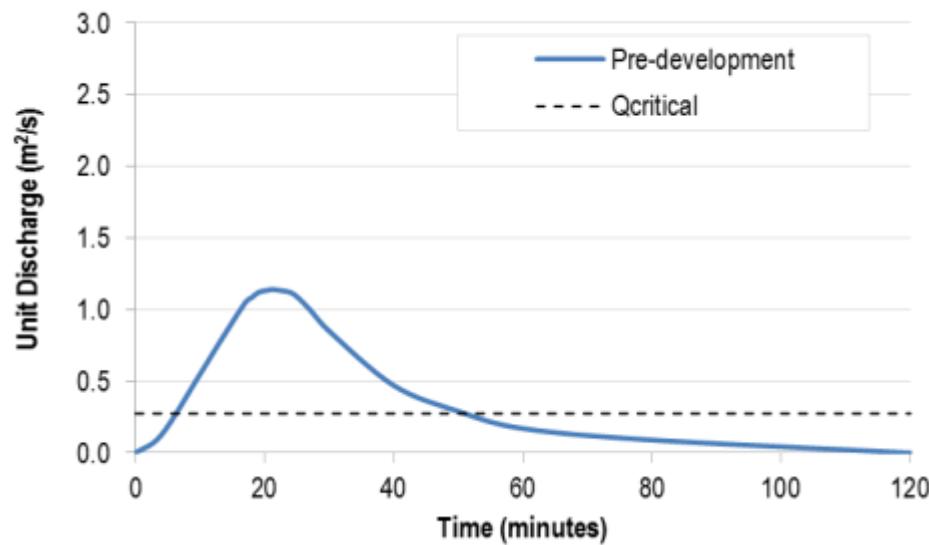
Stormwater Management

Stream restoration in urban catchments through redesigning
stormwater systems: looking to the catchment to save the stream

CHRISTOPHER J. WALSH¹

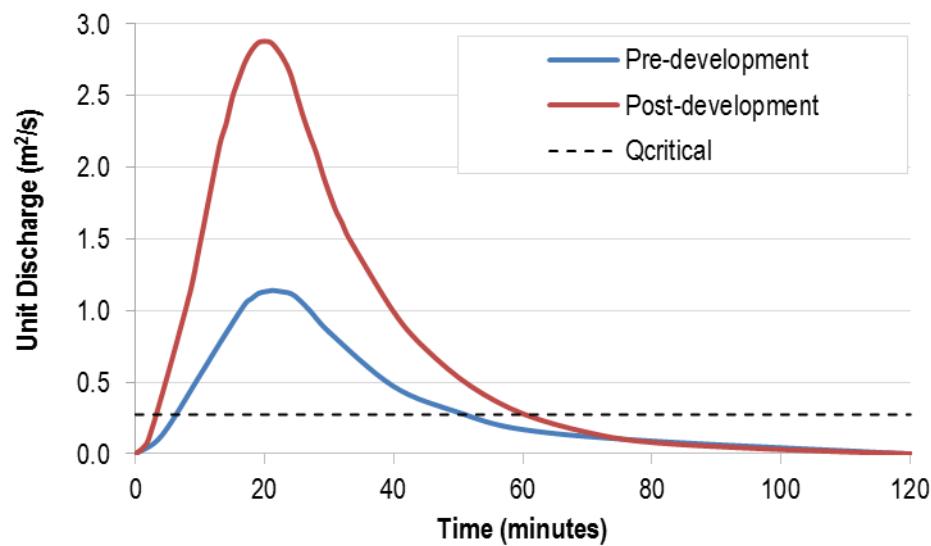
Cooperative Research Centre for Freshwater Ecology, Water Studies Centre, and School of Biological Sciences, Monash University, Victoria 3800, Australia

History of Stormwater Management



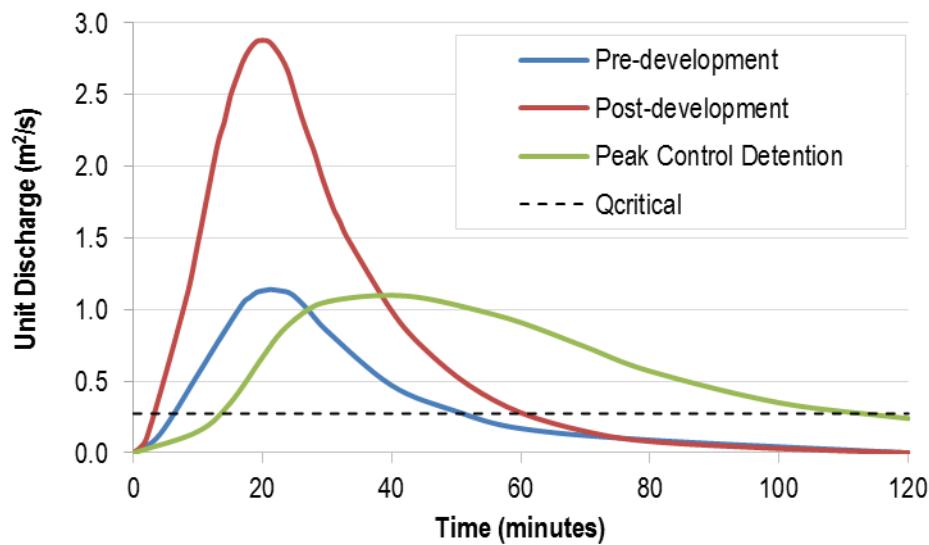
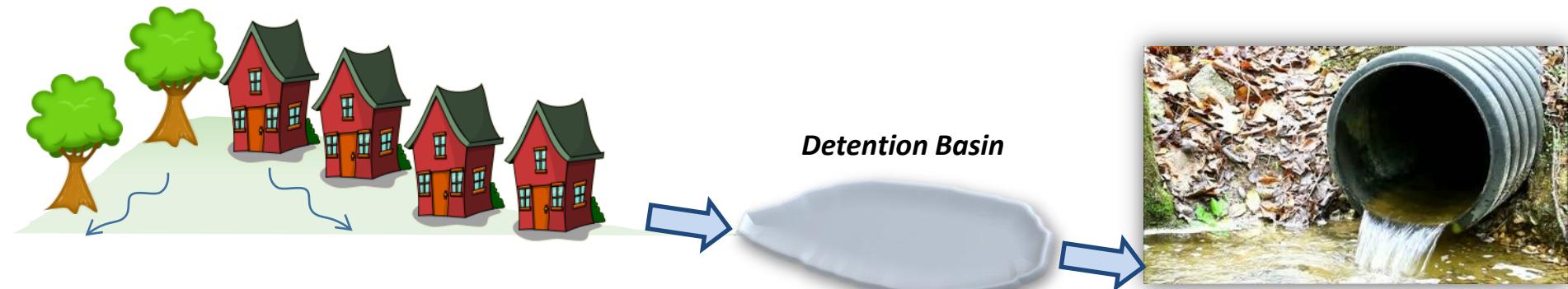
*Analysis of the 2-yr, 2-hr storm from Fort Collins, CO by Bledsoe (2002),
Journal of Water Resources Planning and Management*

~Pre-1950



*Analysis of the 2-yr, 2-hr storm from Fort Collins, CO by Bledsoe (2002),
Journal of Water Resources Planning and Management*

~1980-2000

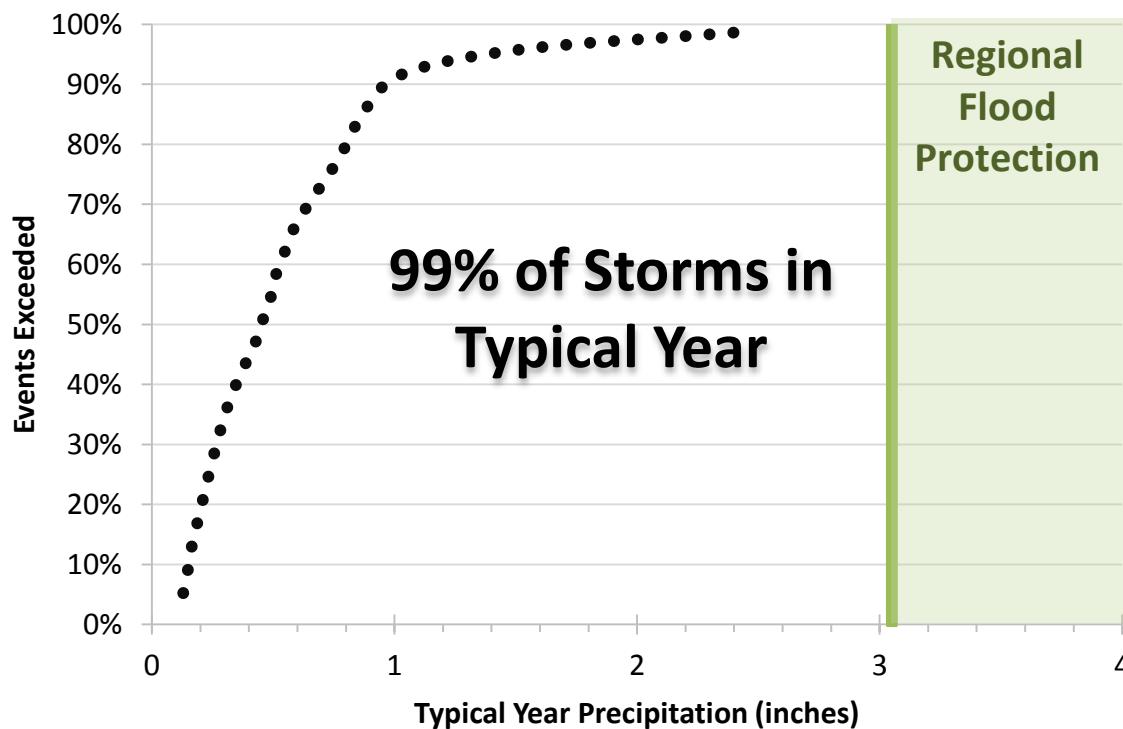


*Analysis of the 2-yr, 2-hr storm from Fort Collins, CO by Bledsoe (2002),
Journal of Water Resources Planning and Management*

~1980-2000



Detention Basin



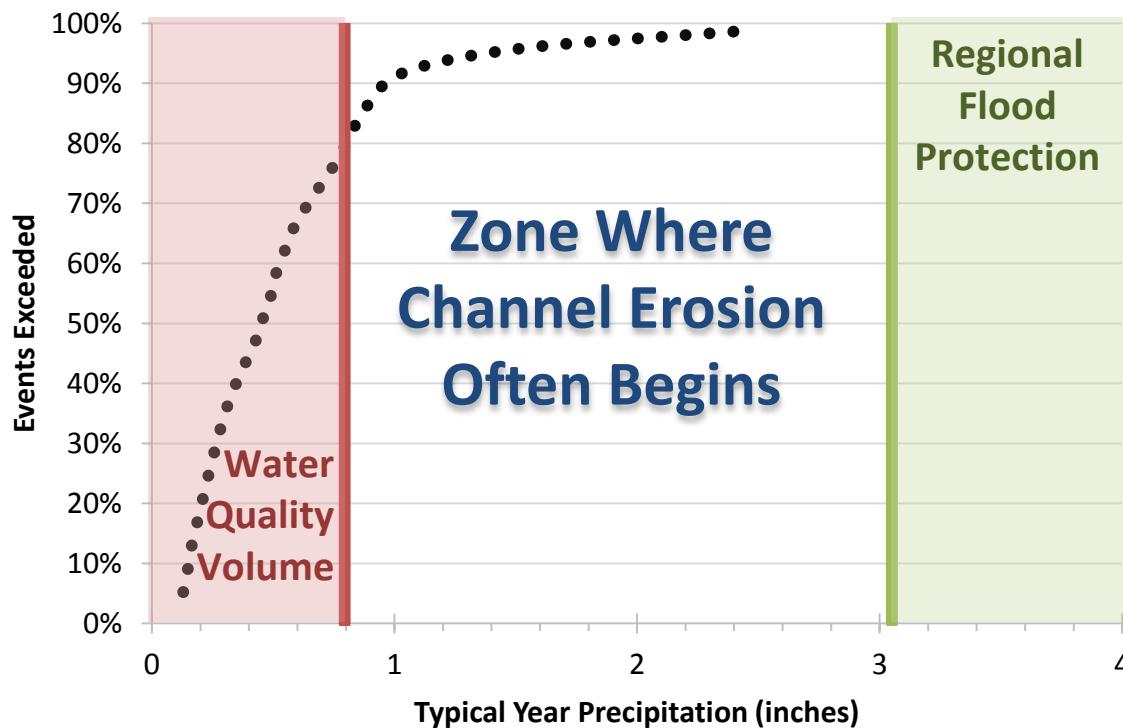
Adapted from Hawley (2012)



~2000-2015



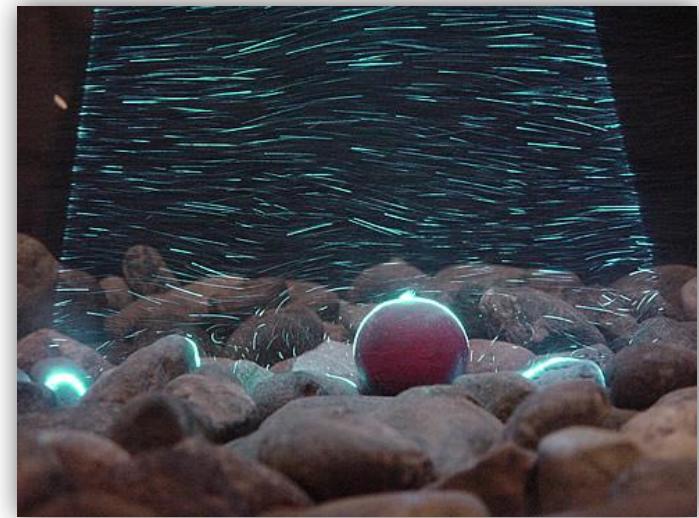
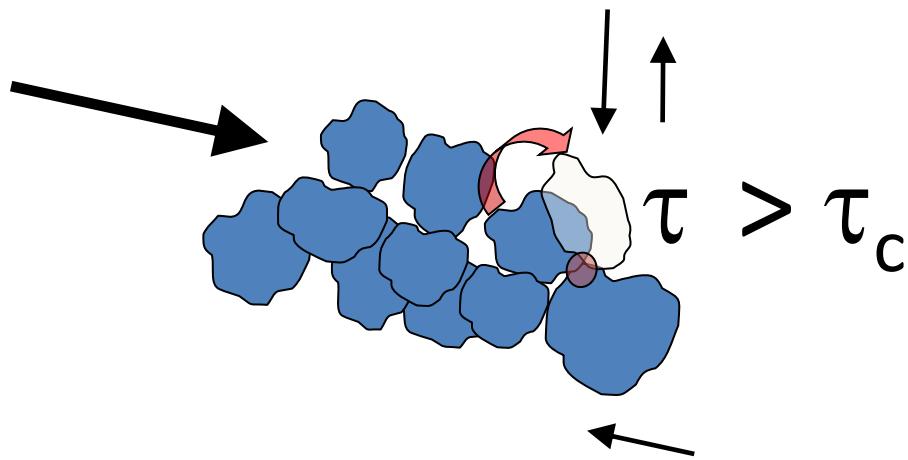
*Extended Detention Basin
with Sediment Forebay*



Adapted from Hawley (2012)

Introduction of Q_{critical}

The Critical Flow for Stream Bed Erosion



Bed Material Transport & Incipient Motion

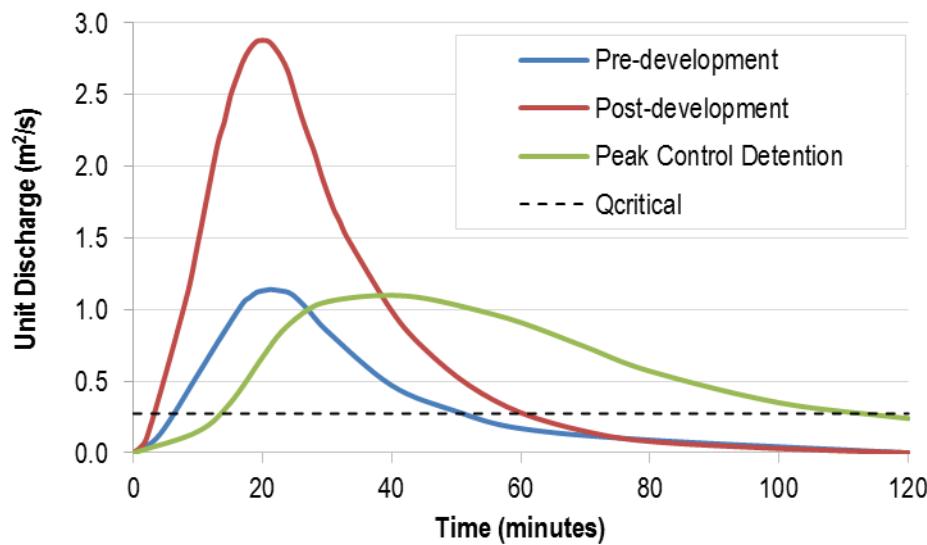
Video Courtesy of John Gaffney (2009) SAFL & NCED, U.Minn



~2000-2015

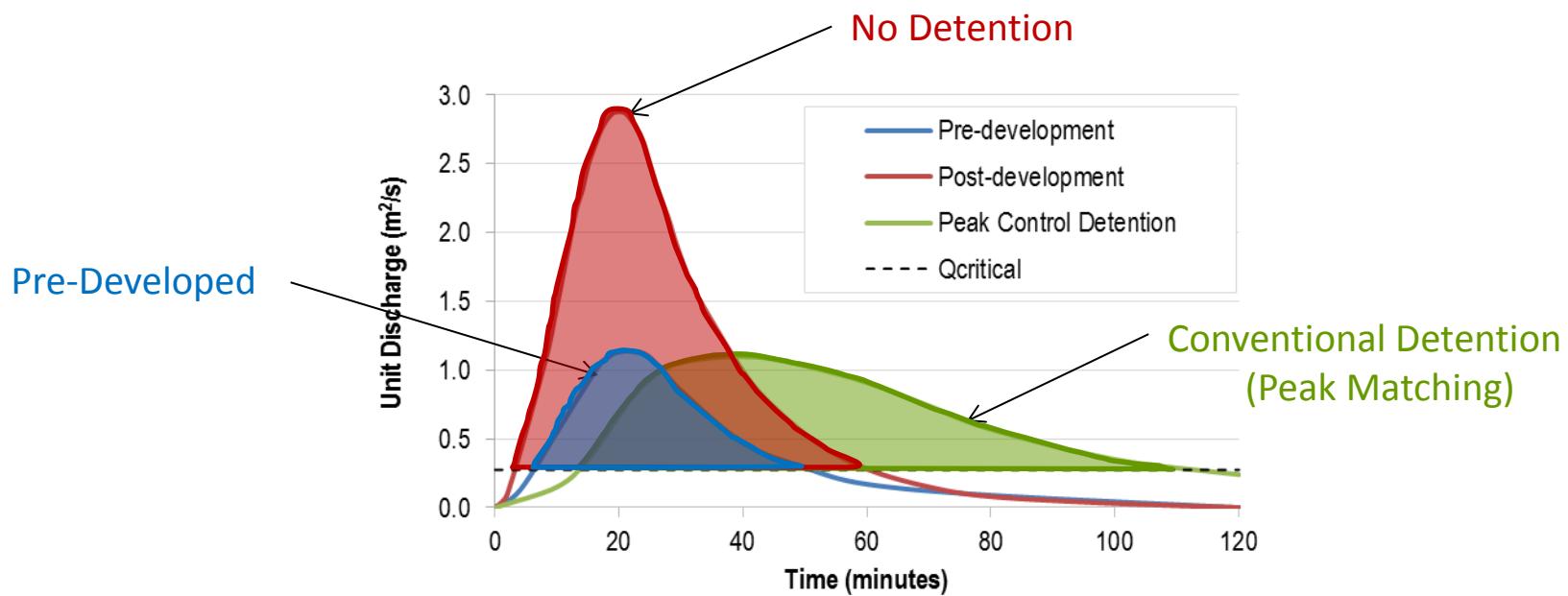
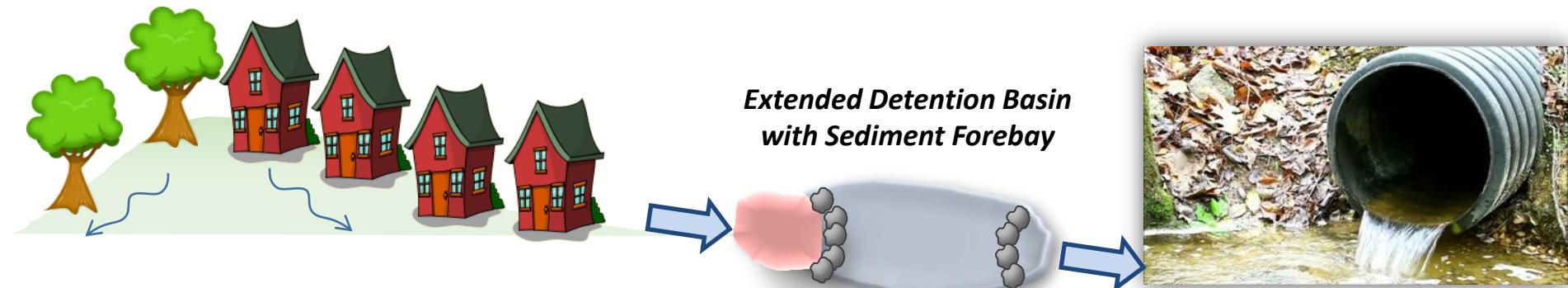


*Extended Detention Basin
with Sediment Forebay*



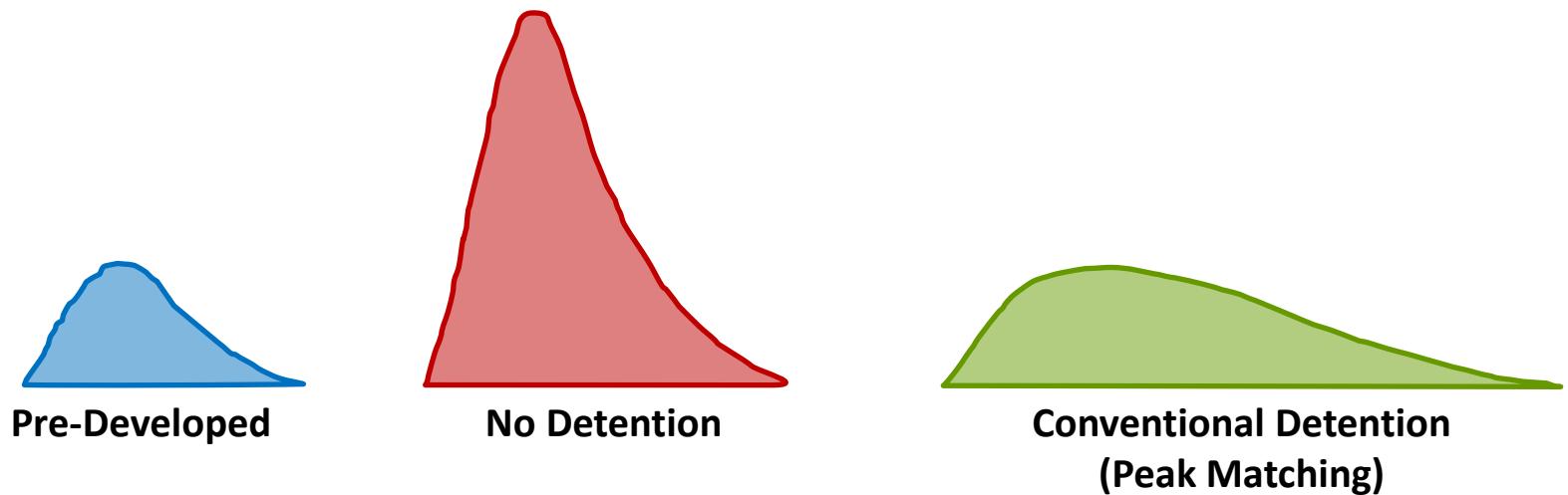
*Analysis of the 2-yr, 2-hr storm from Fort Collins, CO by Bledsoe (2002),
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~2000-2015

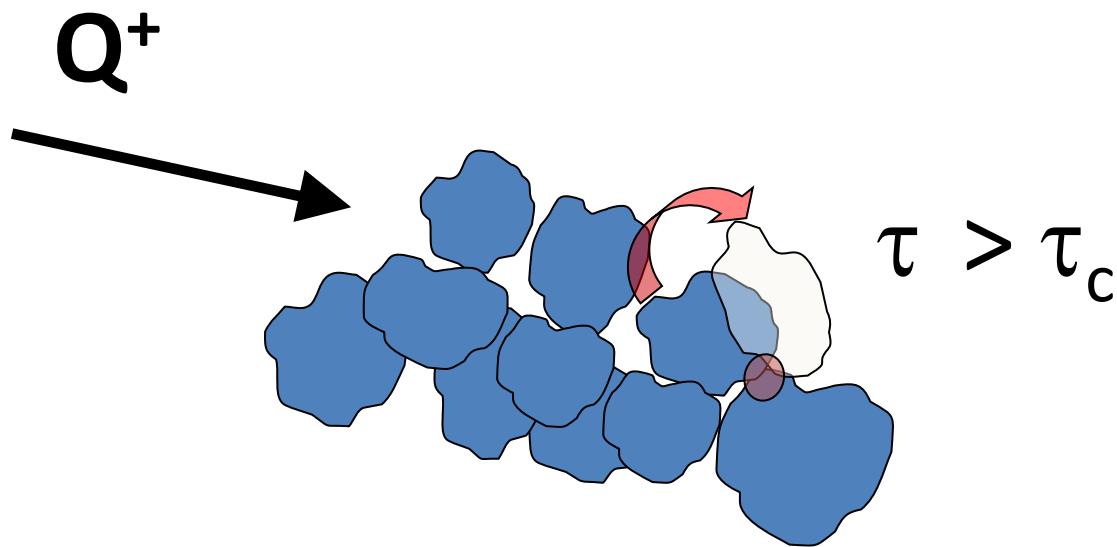


Analysis of the 2-yr, 2-hr storm from Fort Collins, CO by Bledsoe (2002),
Journal of Water Resources Planning and Management

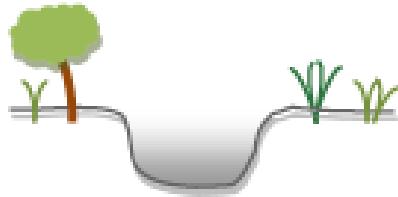
Conventional Detention = More Erosion than Pre-Developed Conditions



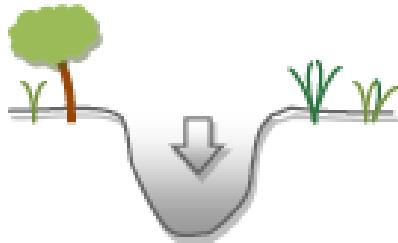
Longer Durations of Flows $> Q_{\text{critical}}$
Increased Transport of Stream Bed Material



Increased Bed Erosion → Incision (Downcutting)

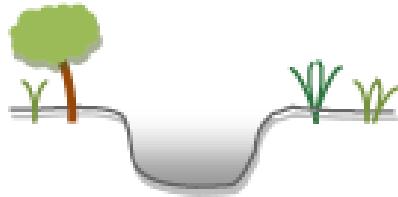


Stage 1 – Equilibrium

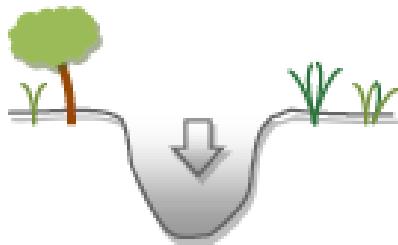


Stage 2 – Incision

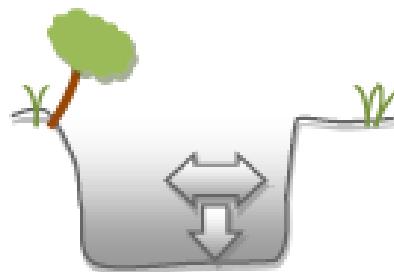
Incision → Taller Banks → Bank Failure



Stage 1 – Equilibrium

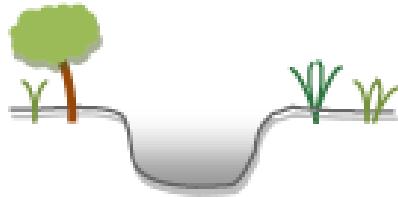


Stage 2 – Incision

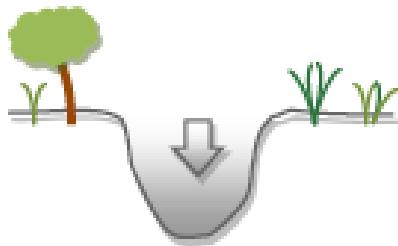


Stage 3 – Widening

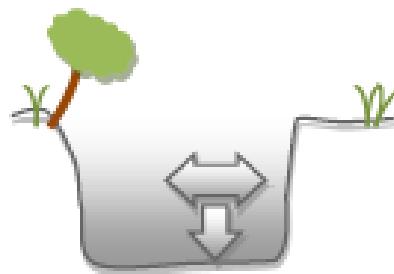
Bank Failure → Widening



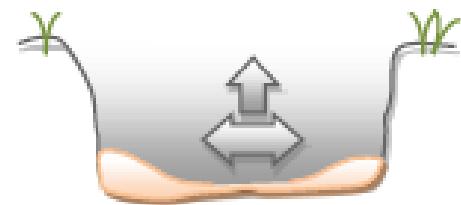
Stage 1 – Equilibrium



Stage 2 – Incision

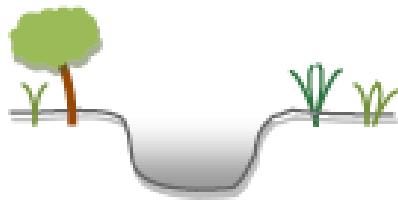


Stage 3 – Widening

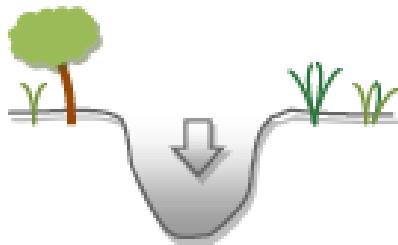


Stage 4 – Aggradation

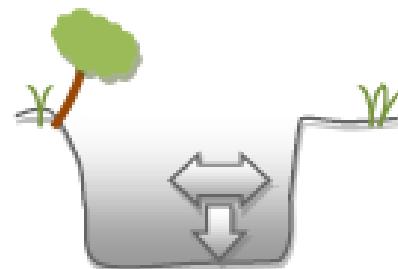
→ Large Amounts of Erosion Before Returning to Equilibrium



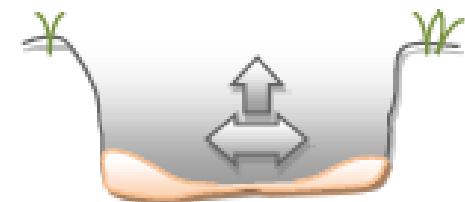
Stage 1 – Equilibrium



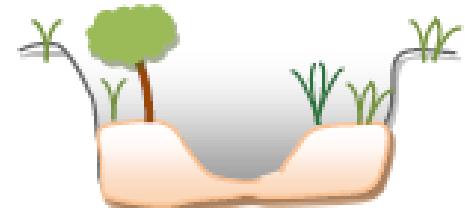
Stage 2 – Incision



Stage 3 – Widening



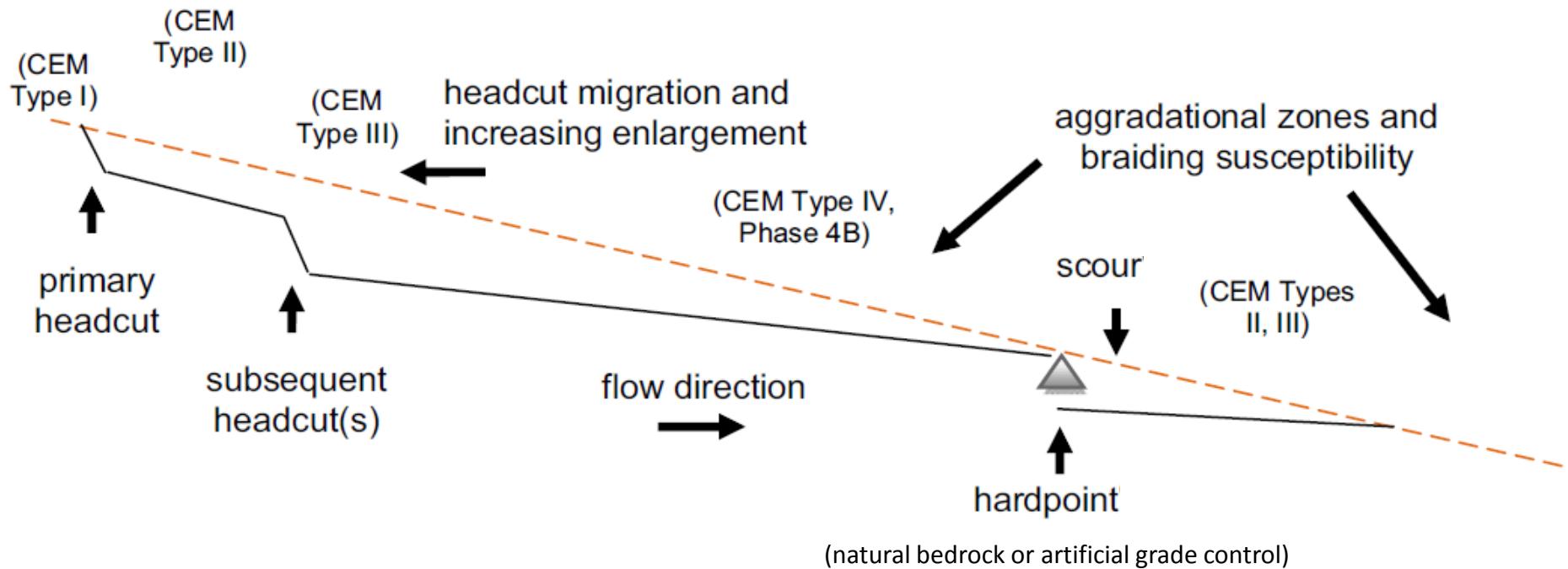
Stage 4 – Aggradation



Stage 5 – Equilibrium

Adapted from Schumm et al. (1984) and Hawley et al. (2012)

Erosion Can Migrate Up and Downstream and Last for Decades or Longer



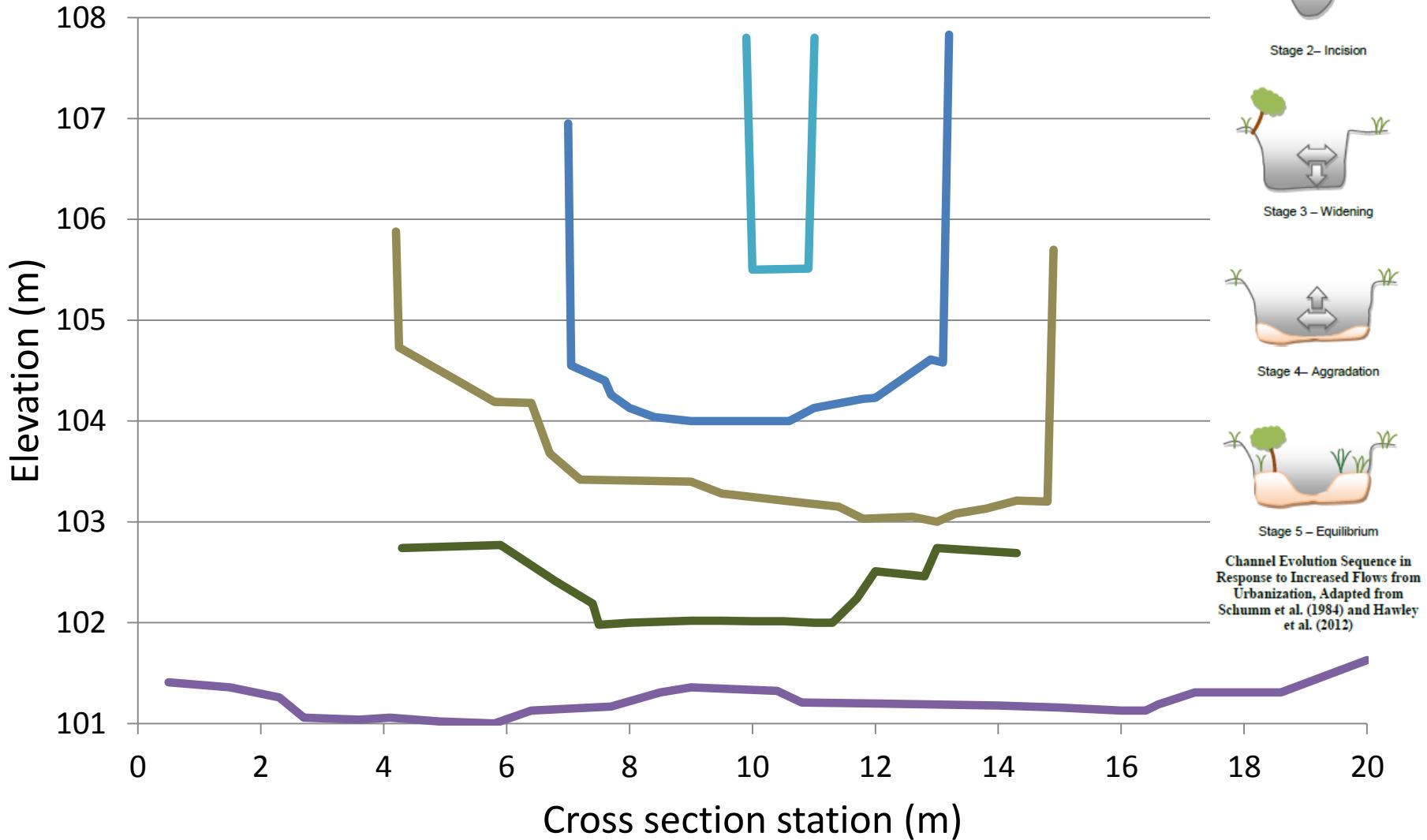
Acton Watershed Case Study (Southern California, USA)

2.5% Imp in 2001, 11% in 2006



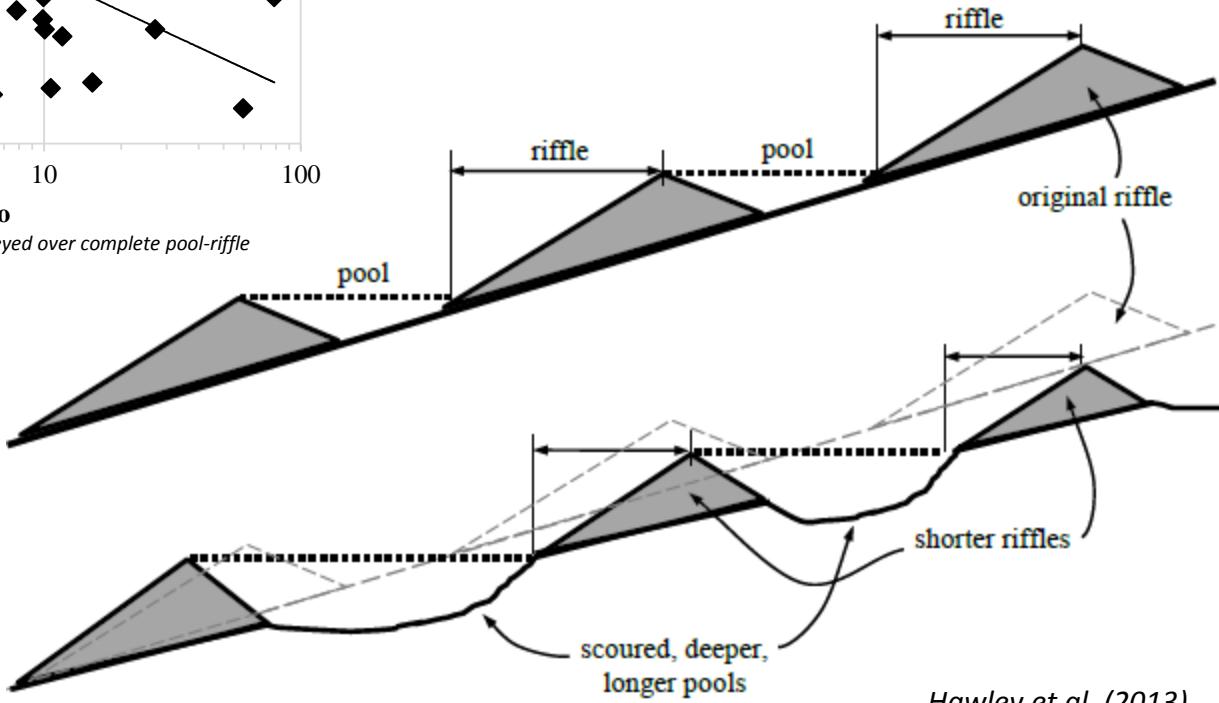
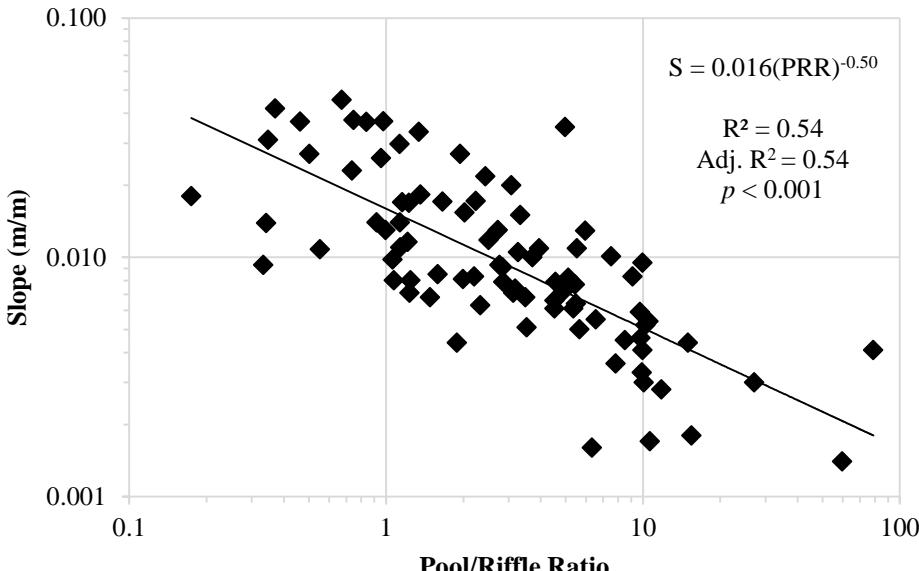
Acton Watershed Case Study (Southern California, USA)

2.5% Imp in 2001, 11% in 2006



Adapted from Hawley and Bledsoe (2013)

Headcutting → Flatter Slopes → Shorter Riffles & Longer Pools

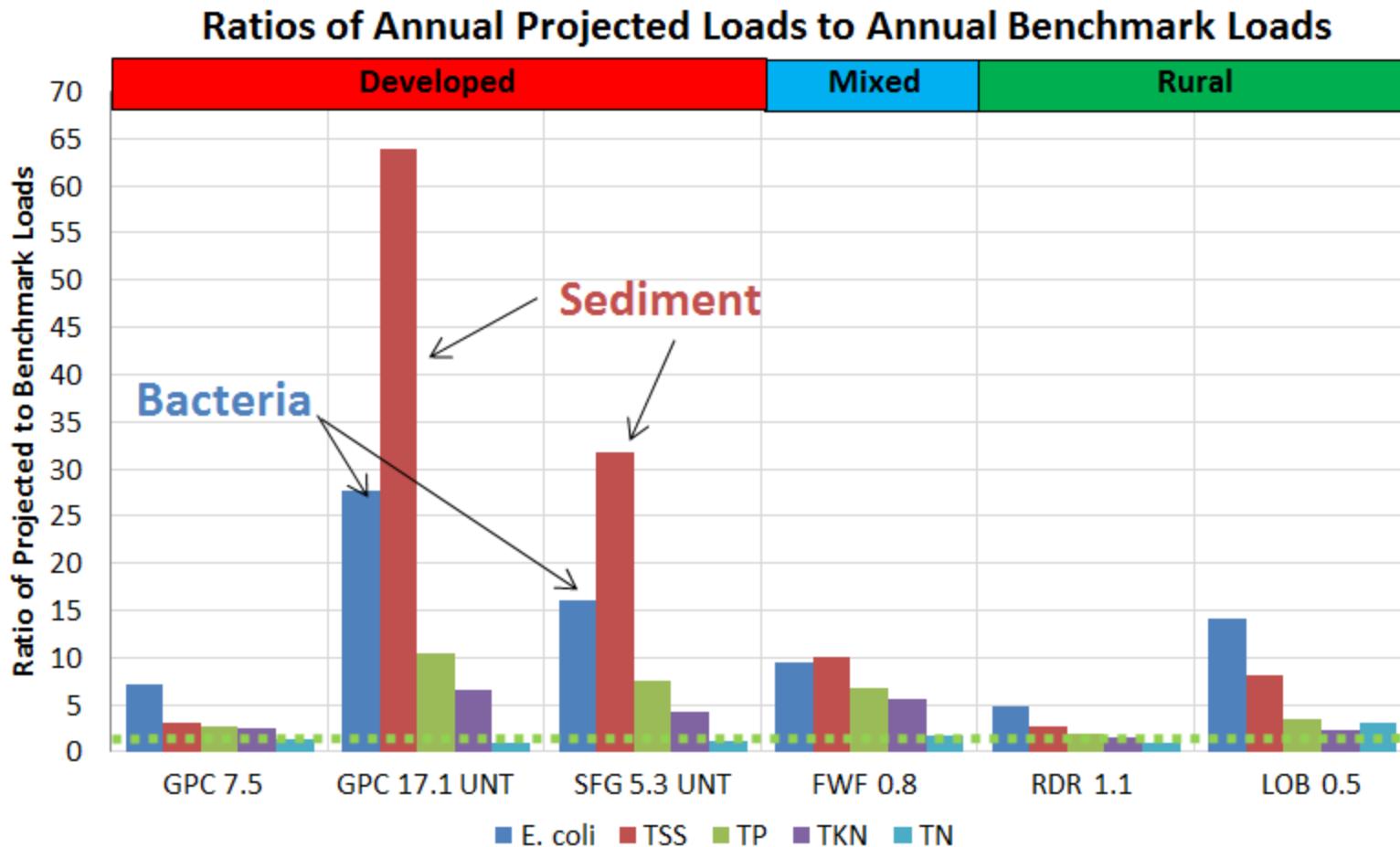


Bank Instability → Fine Sediment Loads

Sediment Is a Leading Impairment of U.S. Waterways



Gunpowder Creek Watershed Case Study (Northern Kentucky, USA)

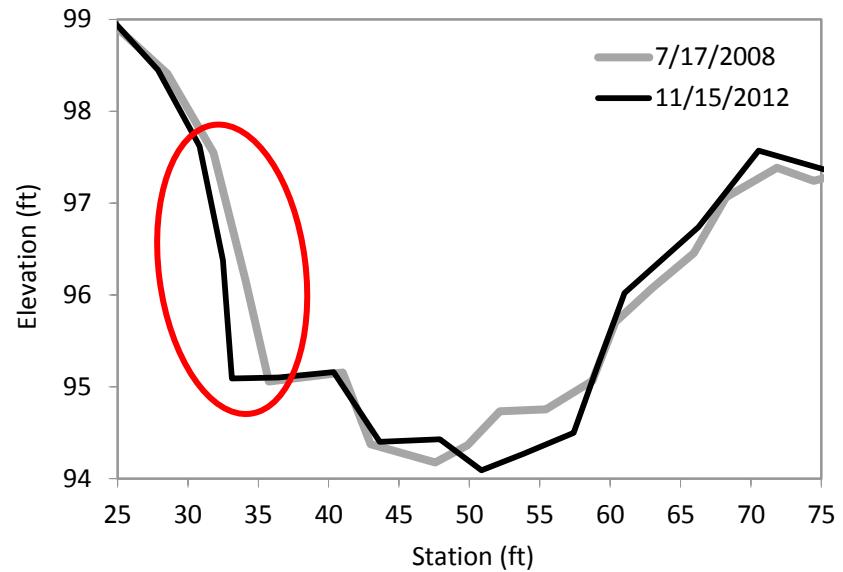


SFG 5.3 - DS

28% impervious



Bank Erosion and Tree Loss



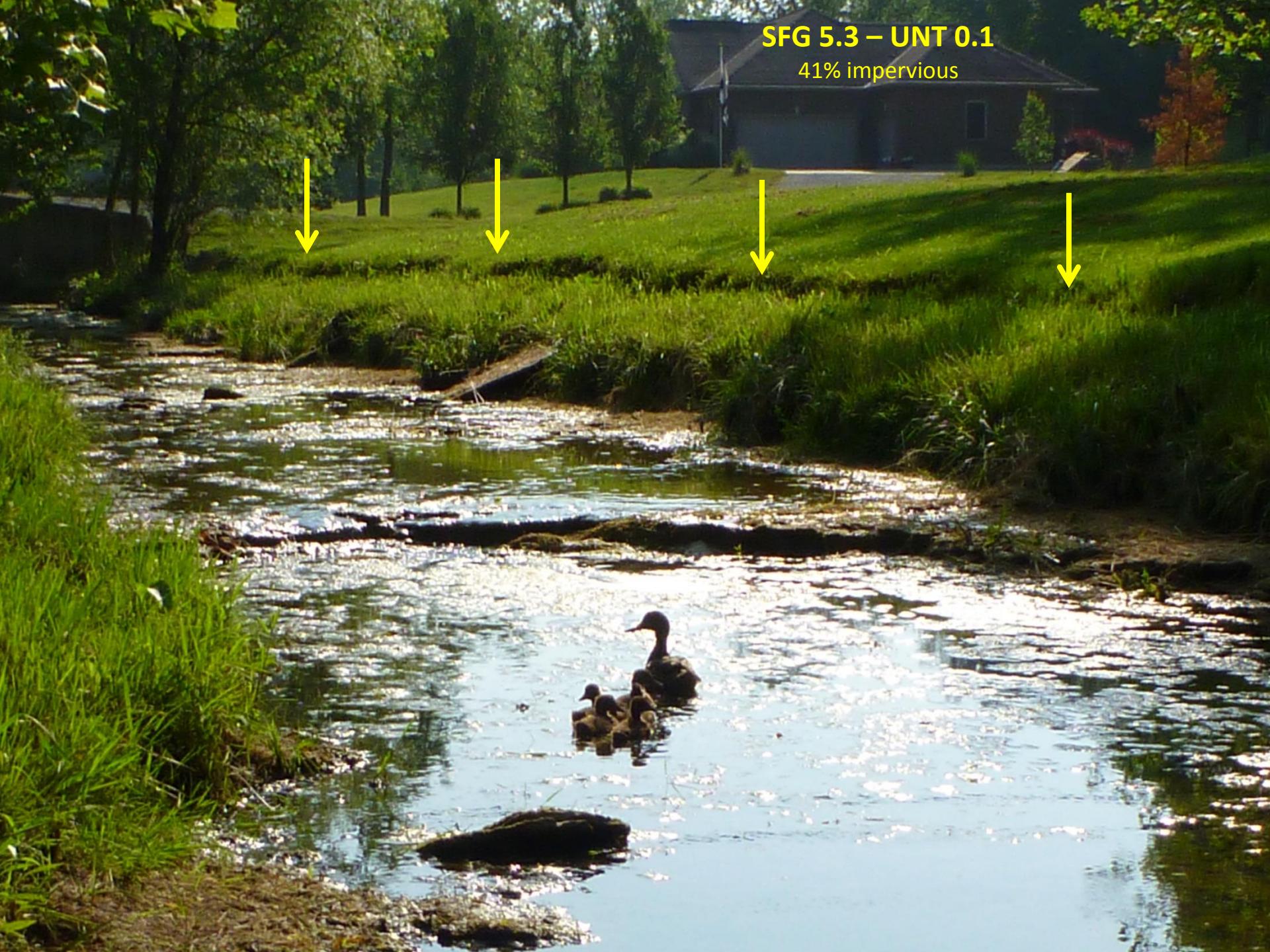
Monitoring Confirms Bank Erosion as a Dominant Source of TSS

Site Name	Projected TSS Yield Due to Bank Erosion (lb/mi ² /yr)	Projected TSS Yield From Water Column Samples (lb/mi ² /yr)	Percent of Projected Load from Bank Erosion
FWF 0.8	76,669	287,089	27%
GPC 7.5	420,123	106,375	395%
LOB 0.5	97,225	192,618	50%
RDR 1.1	148,349	73,749	201%
GPC 17.1 UNT^(a)	0	2,203,207	0%
SFG 5.3 UNT	1,770,761	704,334	251%

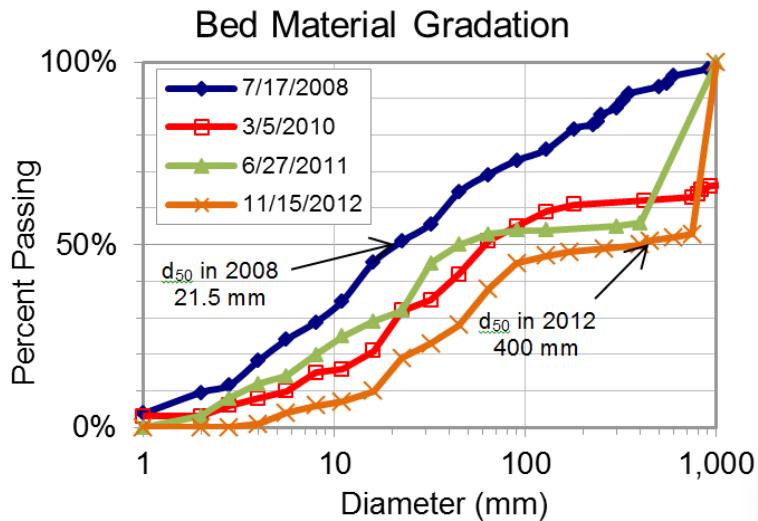
^(a)Bank erosion can be observed at locations throughout the un-named tributary (UNT); however, a log jam at the monitoring site induced sediment deposition and a corresponding bank erosion load of 0. By contrast, the measured bank erosion loads at all other monitoring sites is significant, and in some cases explains more than 100% of the corresponding TSS yields, which supports the treatment of the log jam at GPC 17.1UNT as an outlier.

SFG 5.3 – UNT 0.1

41% impervious



Bed Coarsening and Habitat Homogenization



SFG 5.3 – DS

29% impervious



More homogenous habitat

Conventional Storm Water Designs → Unstable Streams

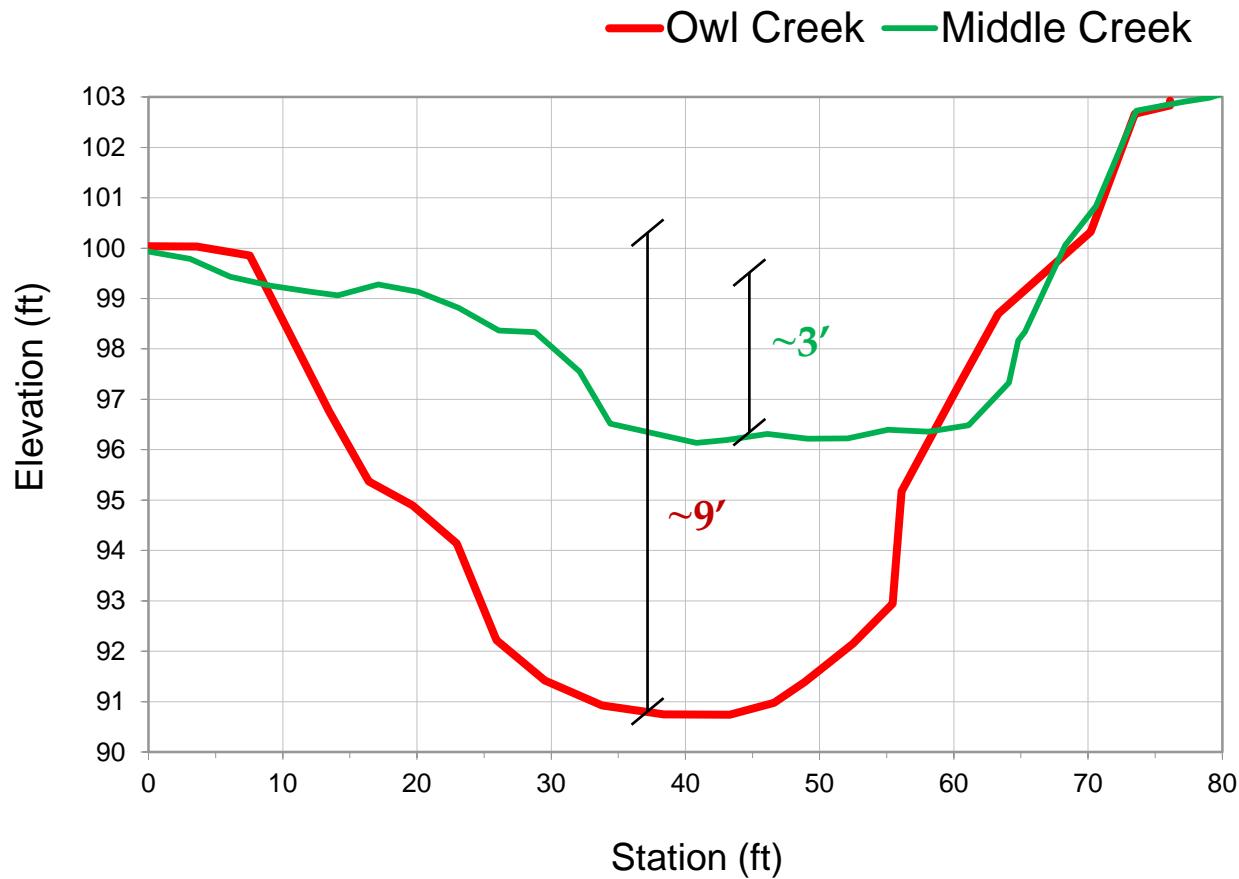


Middle Creek (3.3 mi²)
0.6% Impervious



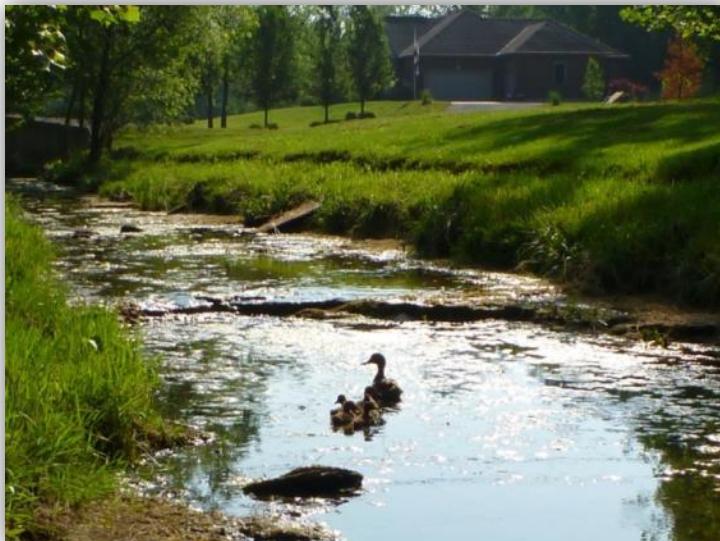
Owl Creek (3.7 mi²)
9% Impervious

Conventional Storm Water Designs → Unstable Streams

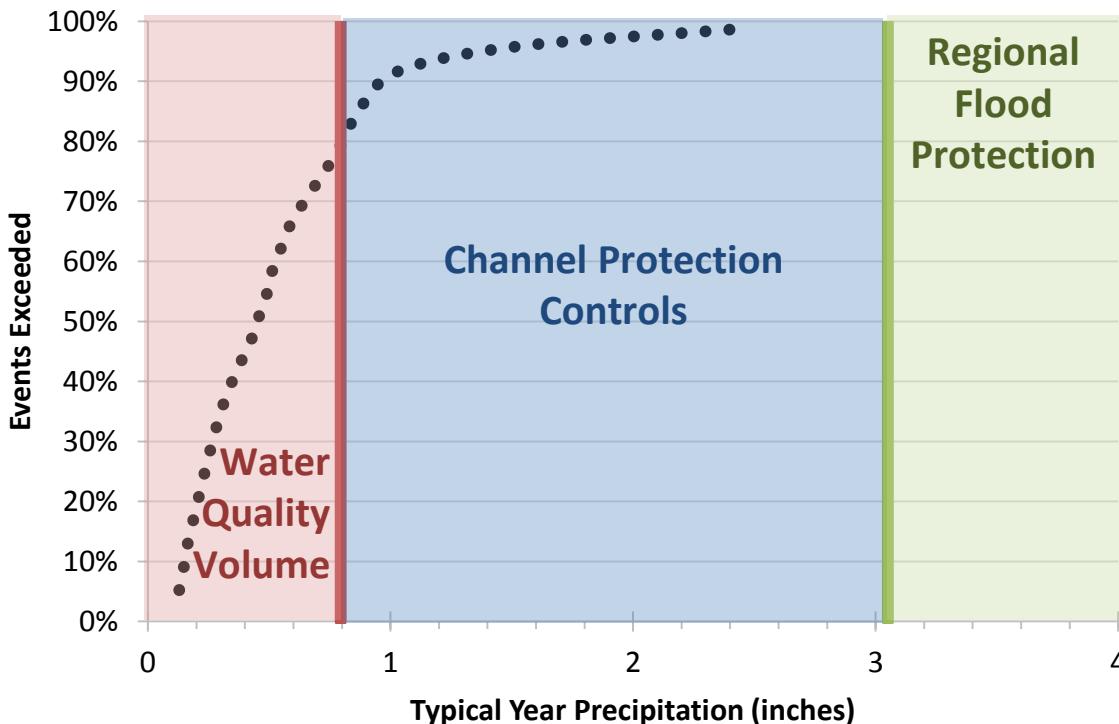
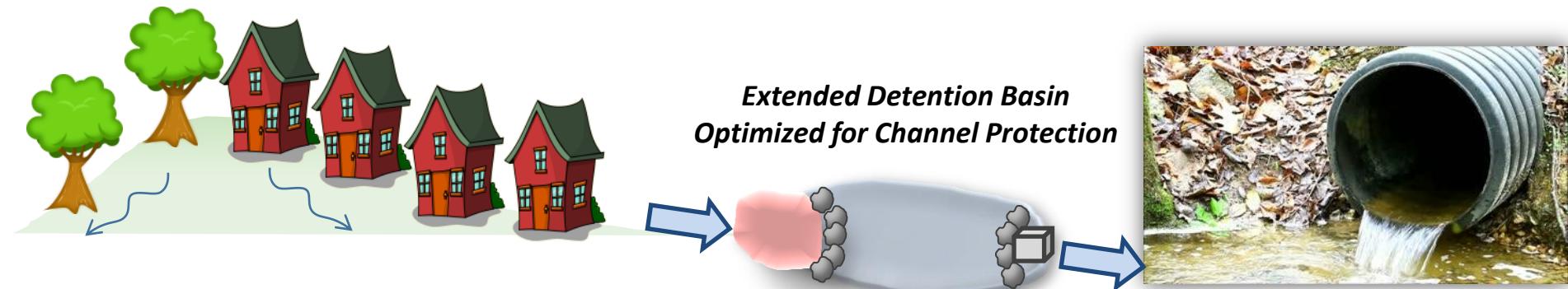


Unstable Streams Impact Resources and Waste \$\$\$

- Aquatic habitat
- Water quality
- Private property
- Infrastructure



Future of Stormwater Management

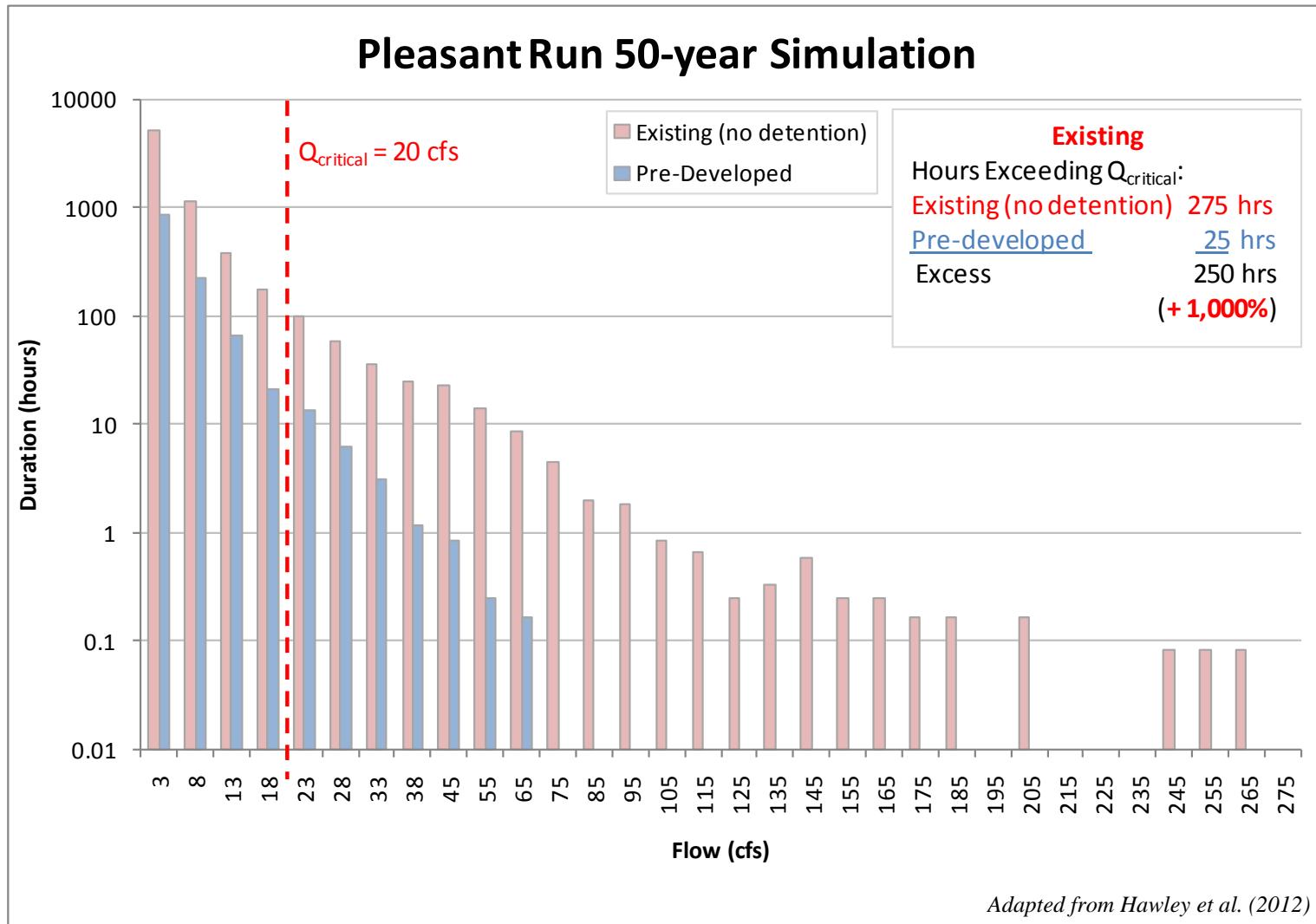


Adapted from Hawley (2012)

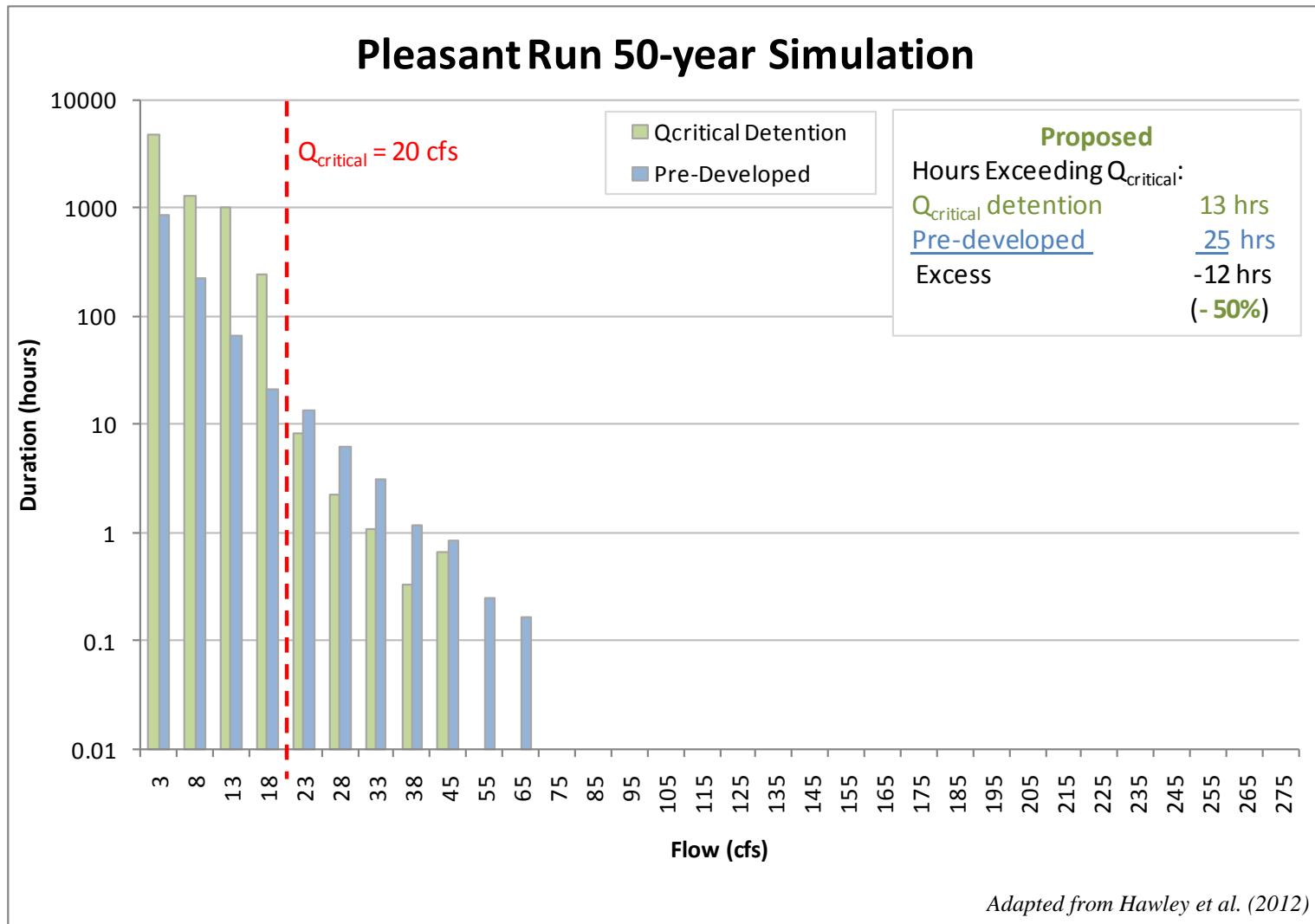
Channel Protection Controls Optimized to Prevent Excess Erosion



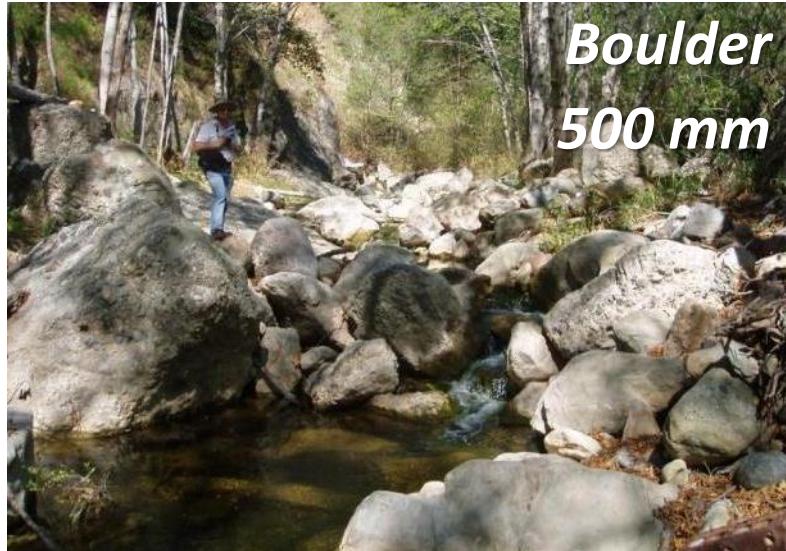
$Q_{critical}$ Design Target = “Safe Release Rate”



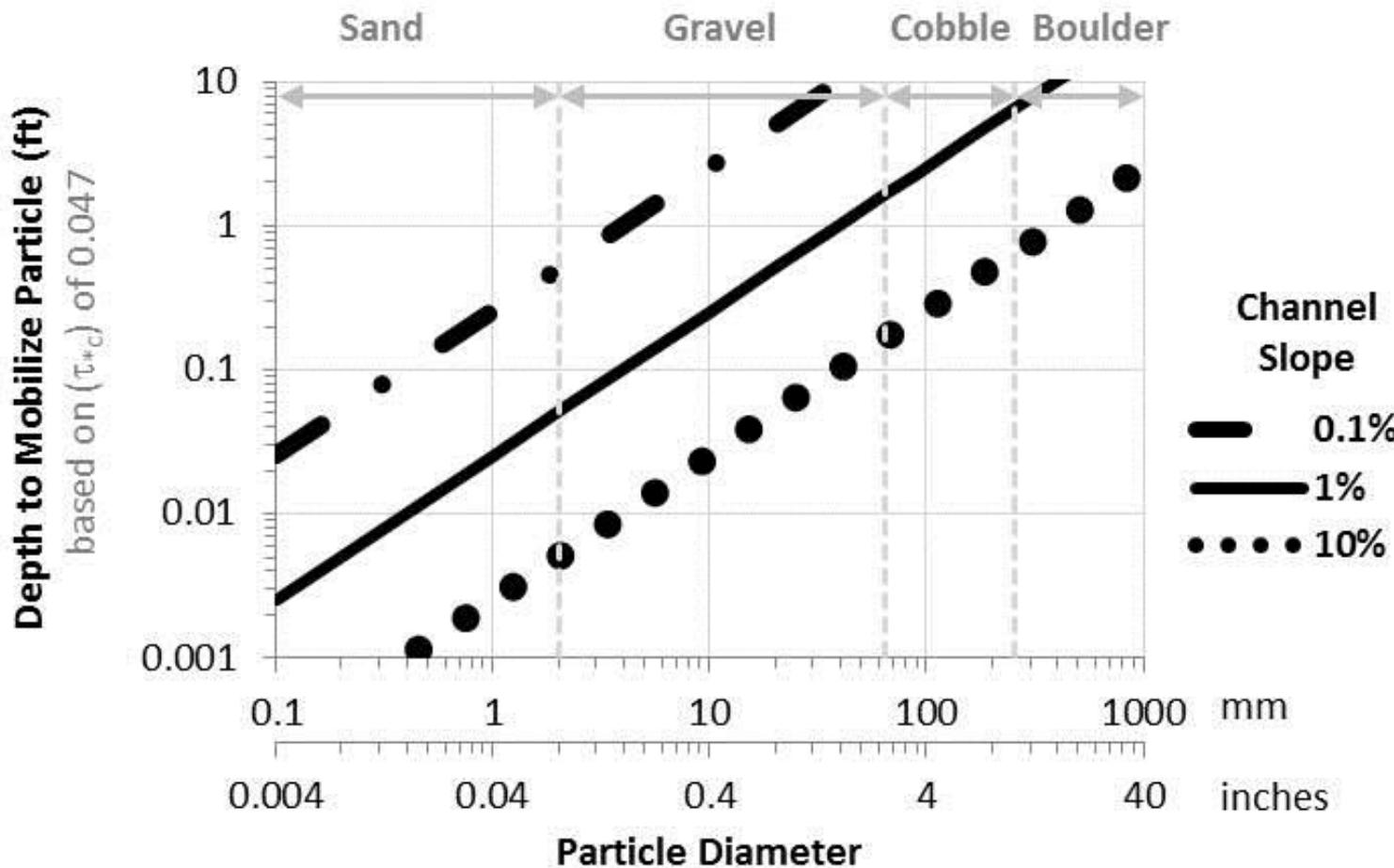
If Excess Volume Is Released Below $Q_{critical}$ → No Excess Erosion or Biological Disturbance



$Q_{critical}$ Varies by Stream Resistance

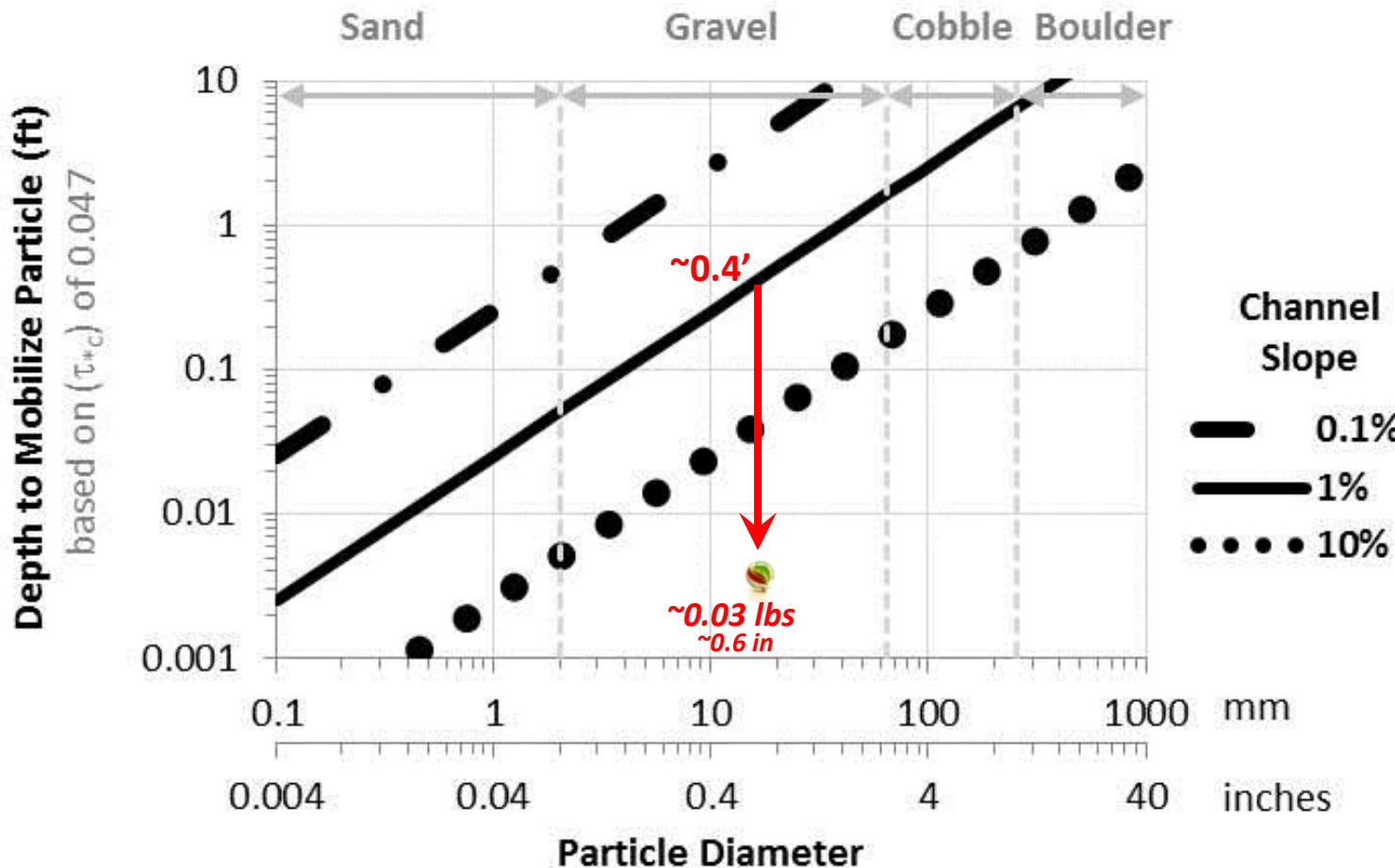


Resistance Increases with Particle Size and Decreases with Slope



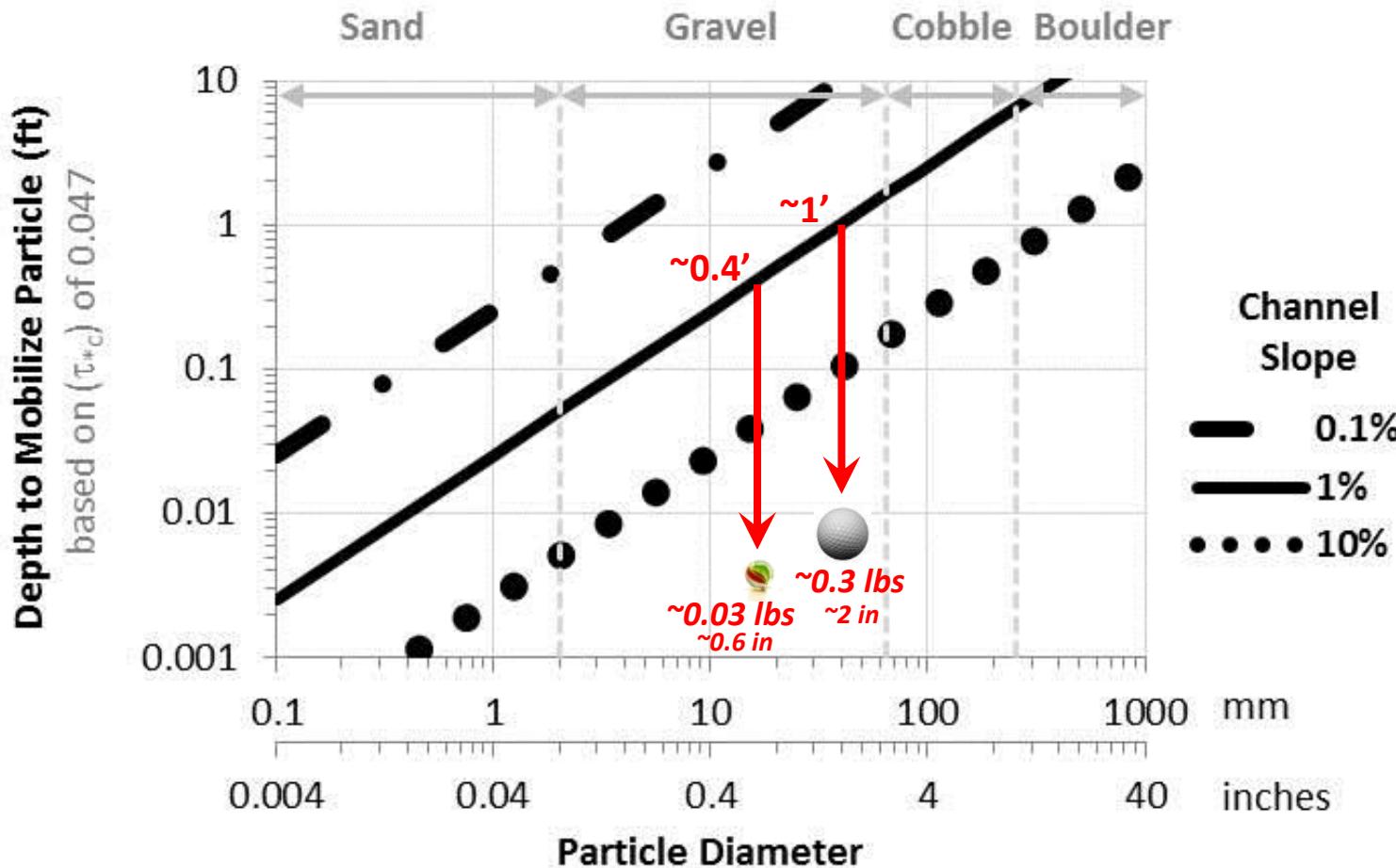
Adapted from Hawley and Vietz (In Press, Freshwater Science)

Resistance Increases with Particle Size and Decreases with Slope



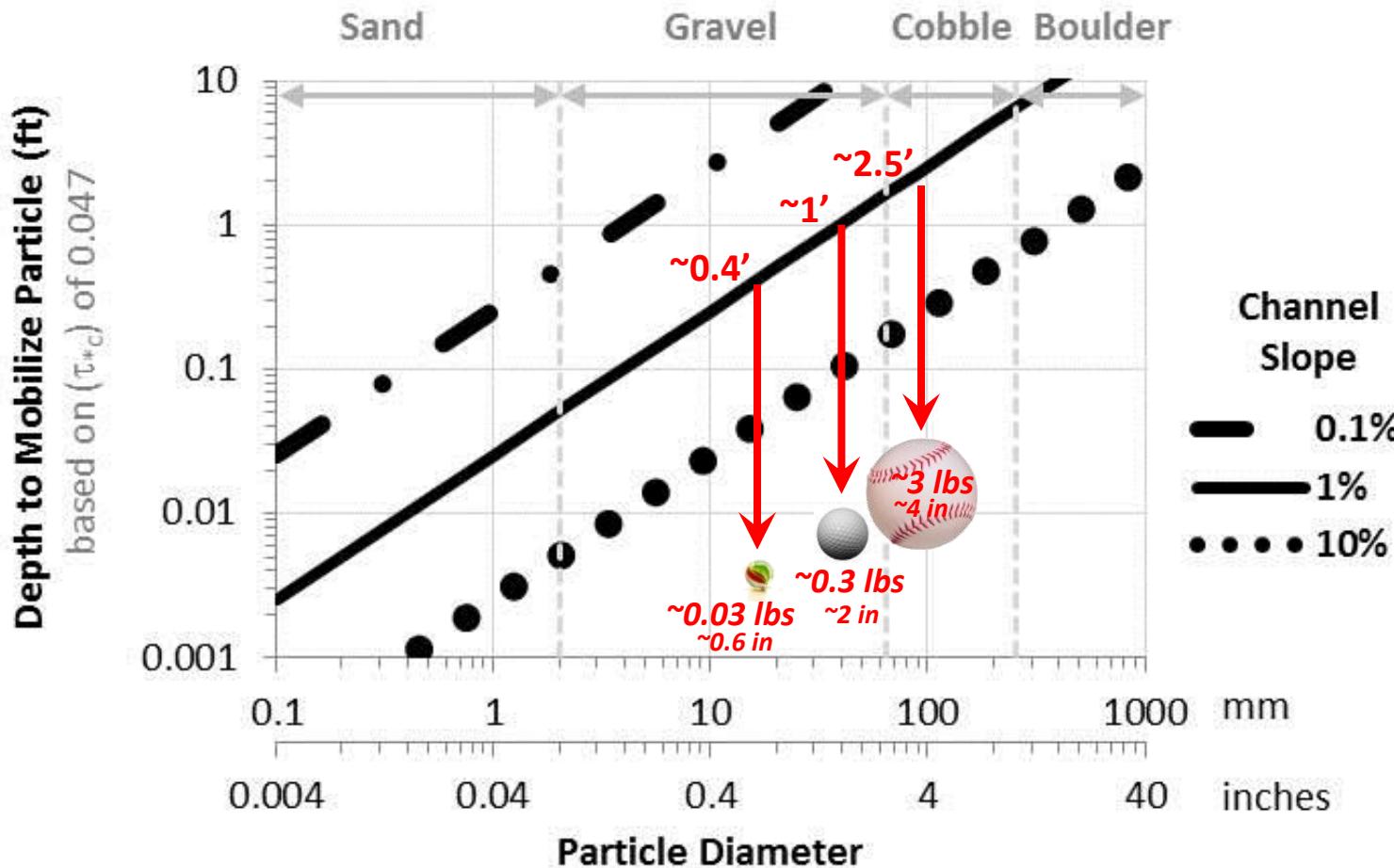
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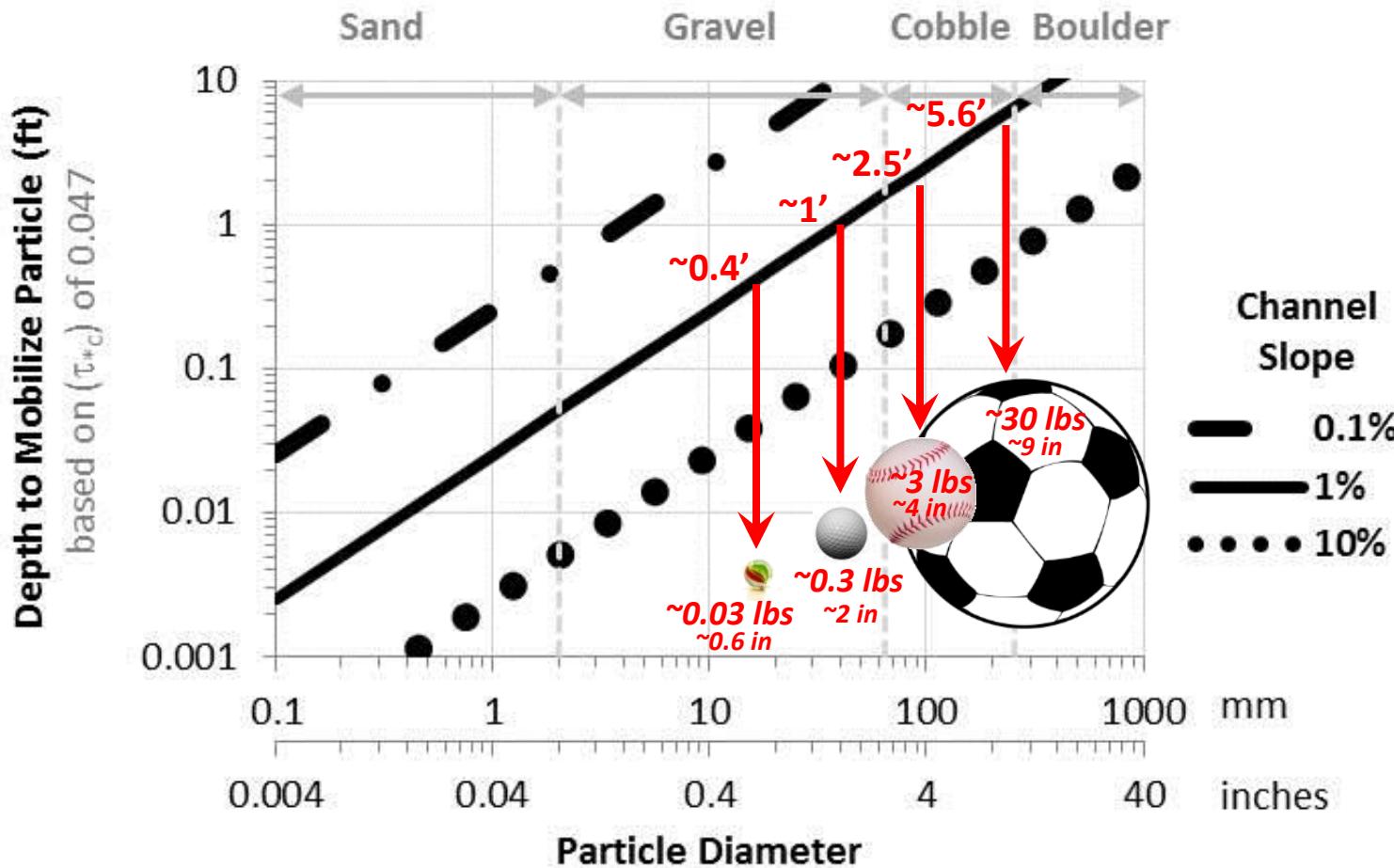
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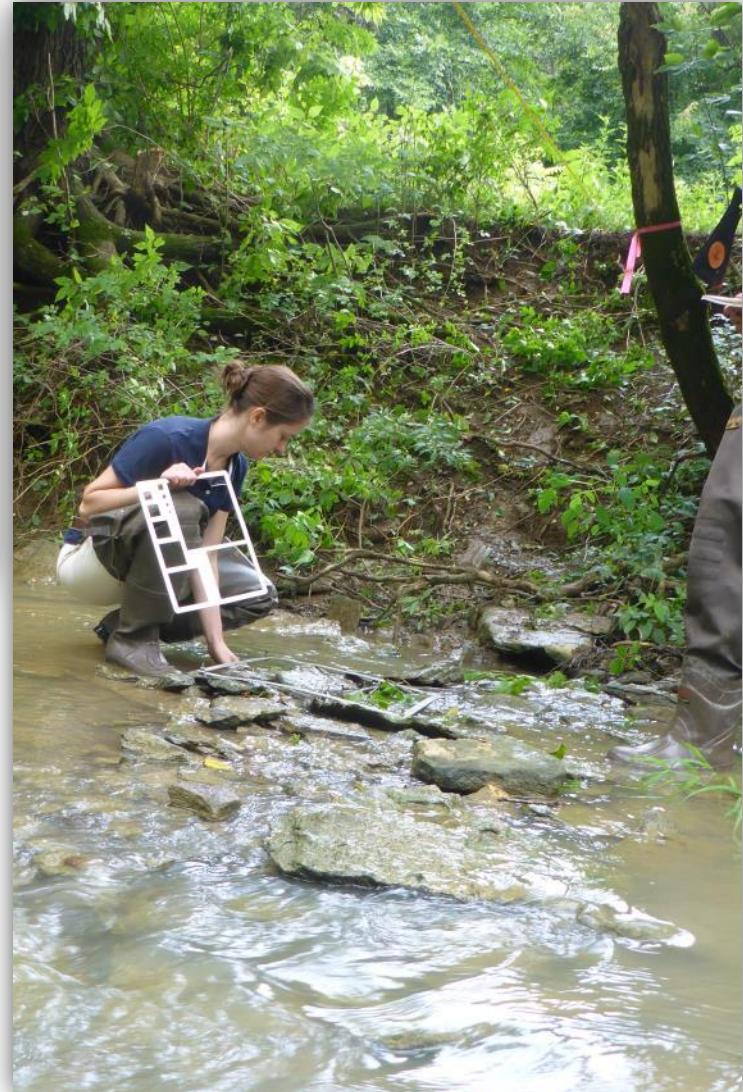
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Resistance Increases with Particle Size and Decreases with Slope

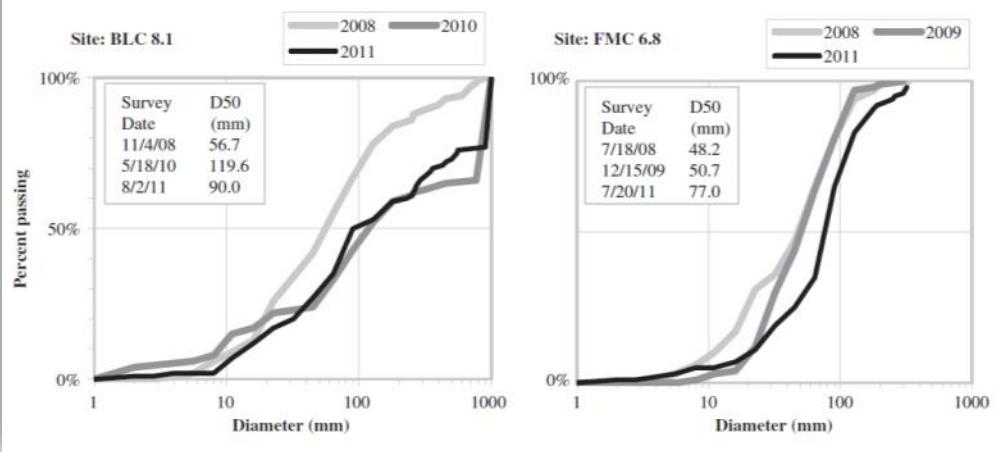


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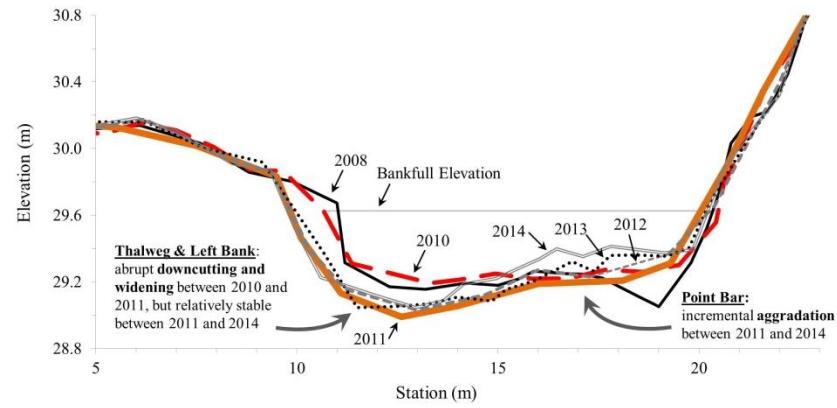
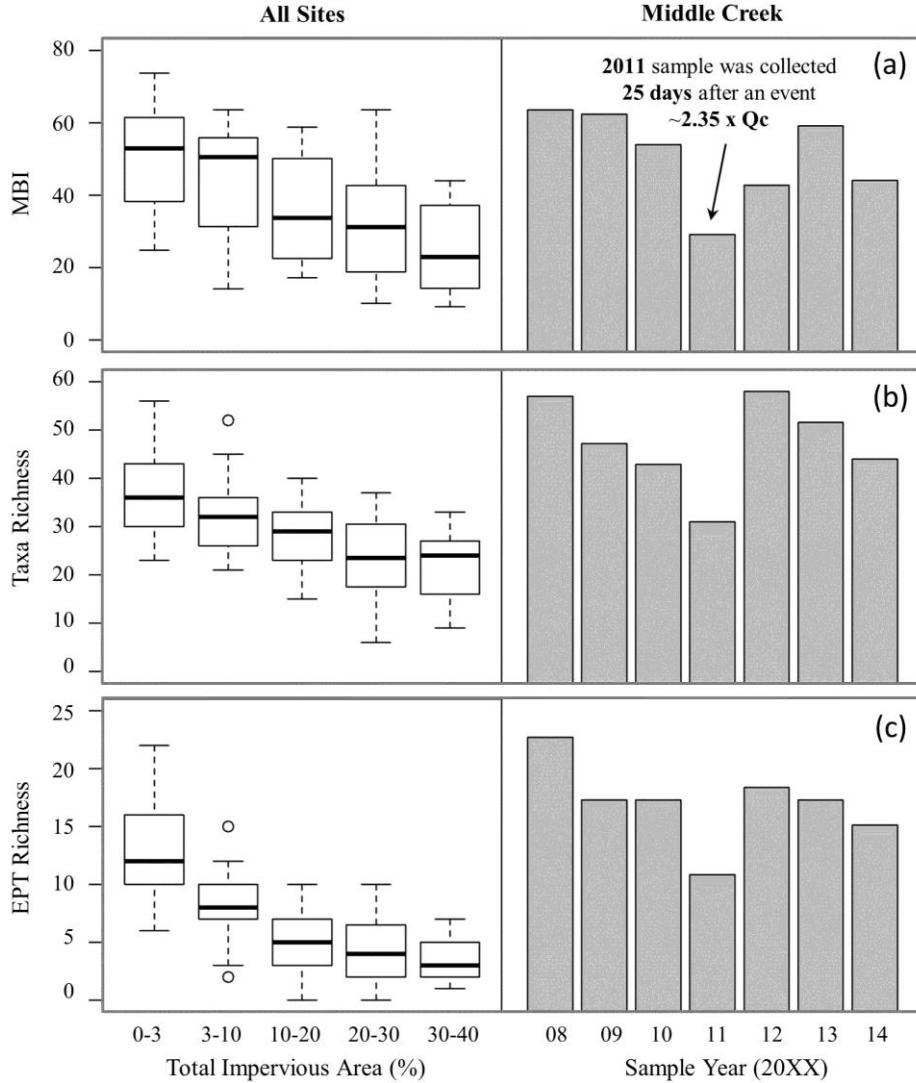
Q_{critical} Needs to Be Calibrated to Stream/Region



R.J. Hawley et al. / Geomorphology 201 (2013) 111–126

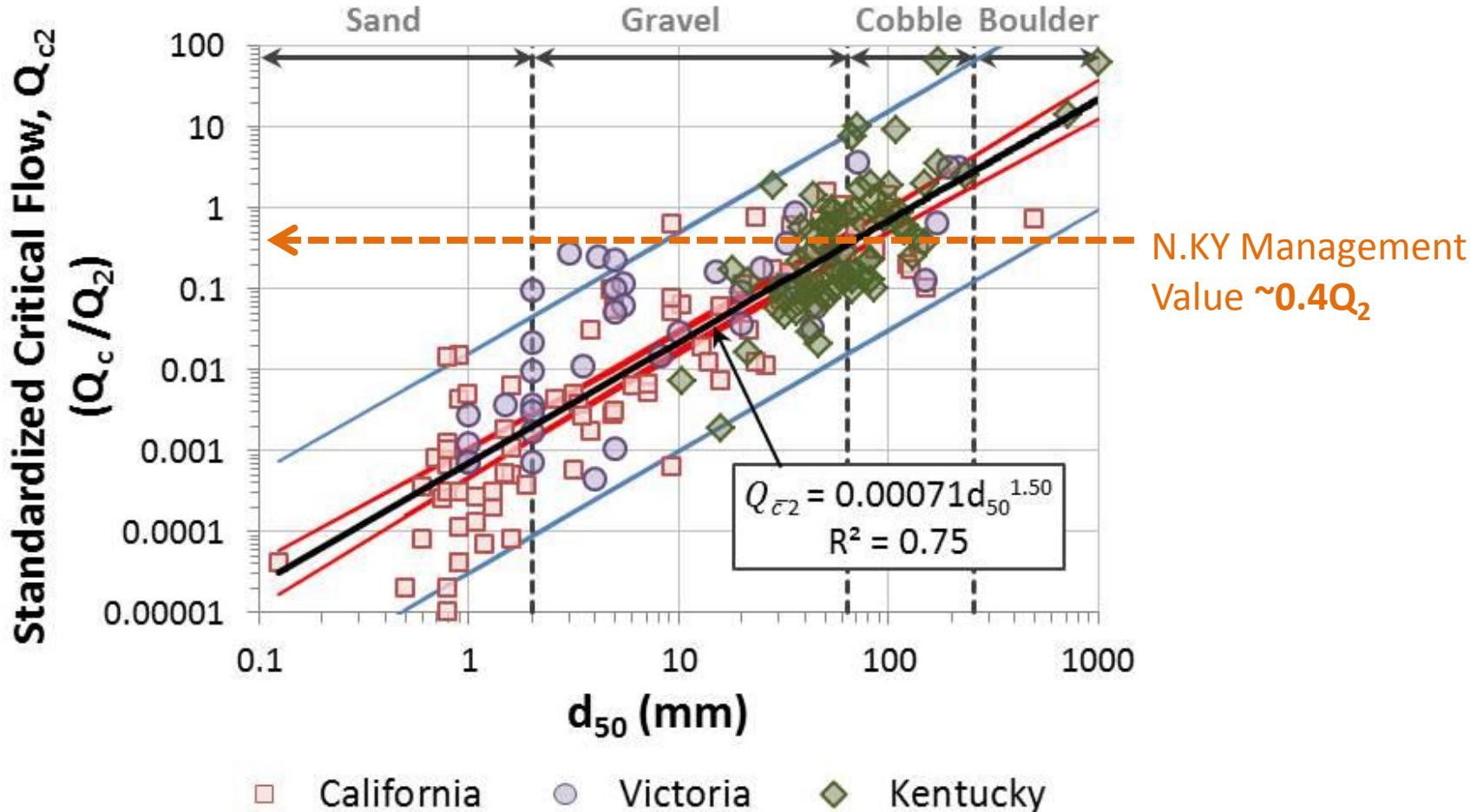


The Importance of $Q_{critical}$ is even Evident at Reference Sites



Adapted from Hawley et al.
(In revision, Freshwater Science)

Q_{critical} Needs to Be Calibrated to Stream/Region



Adapted from Hawley and Vietz (In Press, Freshwater Science)

Optimized N.KY Facilities Can Meet $Q_{critical}$ Target without Becoming Larger

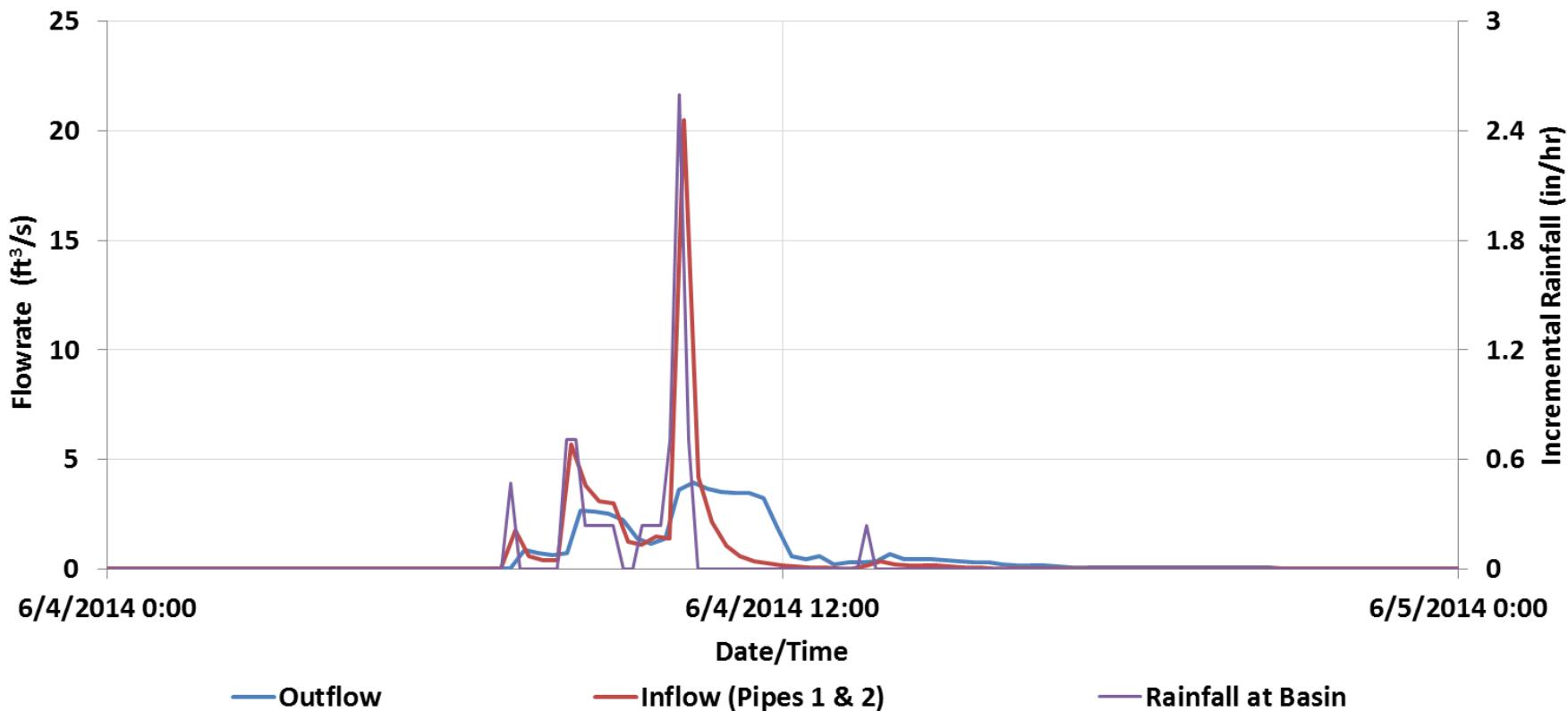
Detention Type	Cumulative Hours $> Q_{critical}$	Cumulative Tons of Sediment Transport
	% Difference from Reference	% Difference from Reference
No Control	903%	1145%
Flood Control Detention	516%	290%
Bioretention with Flood Control and Water Quality	120%	197%
Bioretention with Flood Control, Water Quality, and $Q_{critical}$ Control	32%	-11%

Adapted from Hawley et al. (In prep)

$Q_{critical}$ = Simple Solution for Most Developments in N.KY

(Facilities Draining ≤ 100 acres)

Release 2-yr Storm $< Q_{critical}$



Example 1

Bioretention Basin



Bioretention Basin



Bioretention Basin

- **Step 1: Flood Control**
 - Post \leq Pre for 2-, 10-, 25-, 50-, and 100-year events
- **Step 2: Water Quality Requirements**
 - 0.8 inches of rainfall infiltrates through bioretention soil
- **Step 3: Channel Protection/Q_{critical}**
 - Predevelopment 2-year Peak Flow: 17.89 cfs
 - $Q_{critical} = 0.4 * Q_2$
 - $Q_{critical} = 0.4 * 17.89 \text{ cfs} = 7.16 \text{ cfs}$

Non-optimized Bioretention Basin

Step	Basin Type	Outlet Structure Optimized?	Basin Footprint (SF)	Estimated Excavation (CY)
1. Flood Control Only	Traditional DB	Yes	3,848	2,510
2. Flood/Water Quality	Bioretention	Yes	3,318	2,832
3. Flood/WQ/Q _{critical}	Bioretention	No	5,027	3,846

Poor Optimization from Flood Control and Water Quality Only

- ~50% larger footprint
- ~35% larger volume
- ~0.5 additional design hours

Optimized Bioretention Basin

Step	Basin Type	Outlet Structure Optimized?	Basin Footprint (SF)	Estimated Excavation (CY)
1. Flood Control Only	Traditional DB	Yes	3,848	2,510
2. Flood/Water Quality	Bioretention	Yes	3,318	2,832
3. Flood/WQ/ $Q_{critical}$	Bioretention	Yes	3,318	2,832

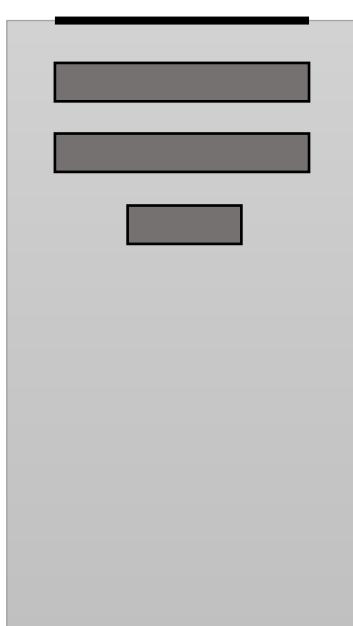
Good Optimization to Meet $Q_{critical}$

- 0% larger footprint
- 0% larger volume
- 2 additional design hours

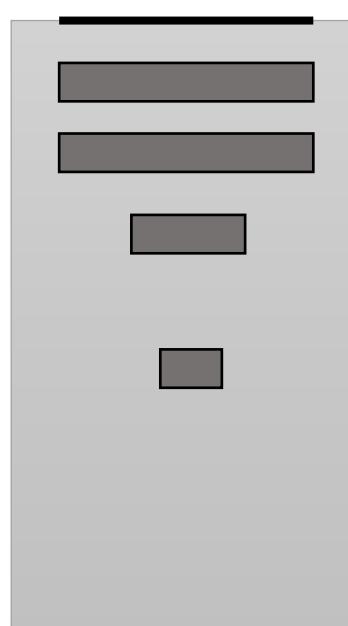
Bioretention Basin

Optimization of Outlet Control Structure

Non-Optimized

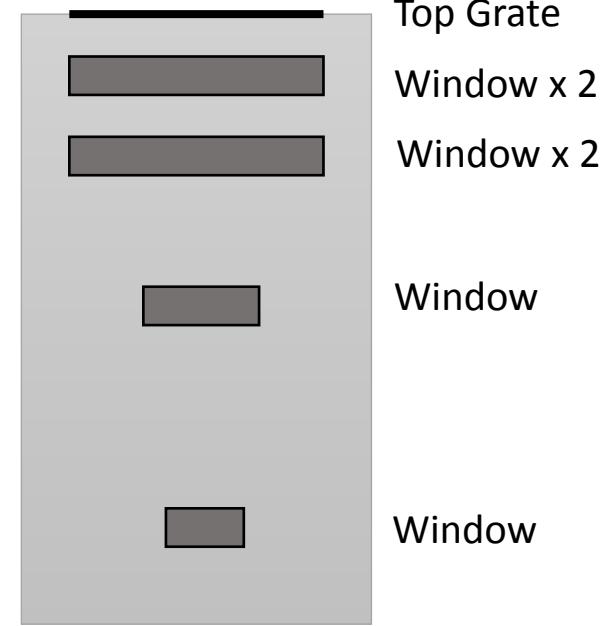


Multiple Iterations



...

Optimized



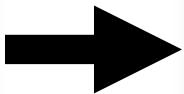
 Underdrain

 Underdrain

 Underdrain

Example 2

Detention Basin Retrofit



Detention Basin Retrofits

Simple change to the outlet control structure



Detention Basin Retrofit

- Maintain Flood Control
- Include Channel Protection
 - $Q_{critical} = 0.4 * 51 \text{ cfs} = 20.6 \text{ cfs}$

Rain Events		Pre-Development	Post-Development with Existing Detention Basin					Post-Development with Modified Detention Basin				
Return Period	Duration		Inflow (cfs)	Inflow (cfs)	Outflow (cfs)	Elevation (feet)	Storage (cubic-feet)	Inflow (cfs)	Outflow (cfs)	Elevation (feet)	Storage (cubic-feet)	
3-Month	24-Hour	7.49		31.24	15.16	834.60	13,060	31.24	6.55	835.35	25,234	
6-Month	24-Hour	18.63		44.33	17.92	835.19	22,040	44.33	12.84	835.84	35,136	
1-Year	24-Hour	34.03		59.55	21.08	835.75	33,259	59.55	16.04	836.41	48,430	
2-Year	24-Hour	51.51		74.87	23.80	836.29	45,572	74.87	20.43	836.96	62,060	
10-Year	24-Hour	104.63		115.77	35.21	837.55	78,844	115.77	34.31	838.20	97,925	
25-Year	24-Hour	139.40		140.28	43.12	838.21	98,422	140.28	40.54	838.89	120,219	
50-Year	24-Hour	168.00		159.72	48.23	838.71	114,329	159.72	45.69	839.40	138,214	
100-Year	24-Hour	198.52		180.01	52.84	839.22	131,607	180.01	50.35	839.92	156,978	

Notes	Notes	Notes
Pre-Development DA = 34.26 acres with CN = 74	Post-Development DA = 22.35 acres with CN = 91 Outlet Pipe Invert (Lower): 832.12 feet Outlet Pipe Invert (Upper): 836.21 feet Spillway Invert: 839.96 feet	The modeling scenario of modified detention basin includes: 1. Flow restriction = 75% through filter media 2. Diameter of bypass wye connection = 18 inches 3. Elevation of bypass wye connection = 835.12 feet

Adapted from Hawley et al. (In review)

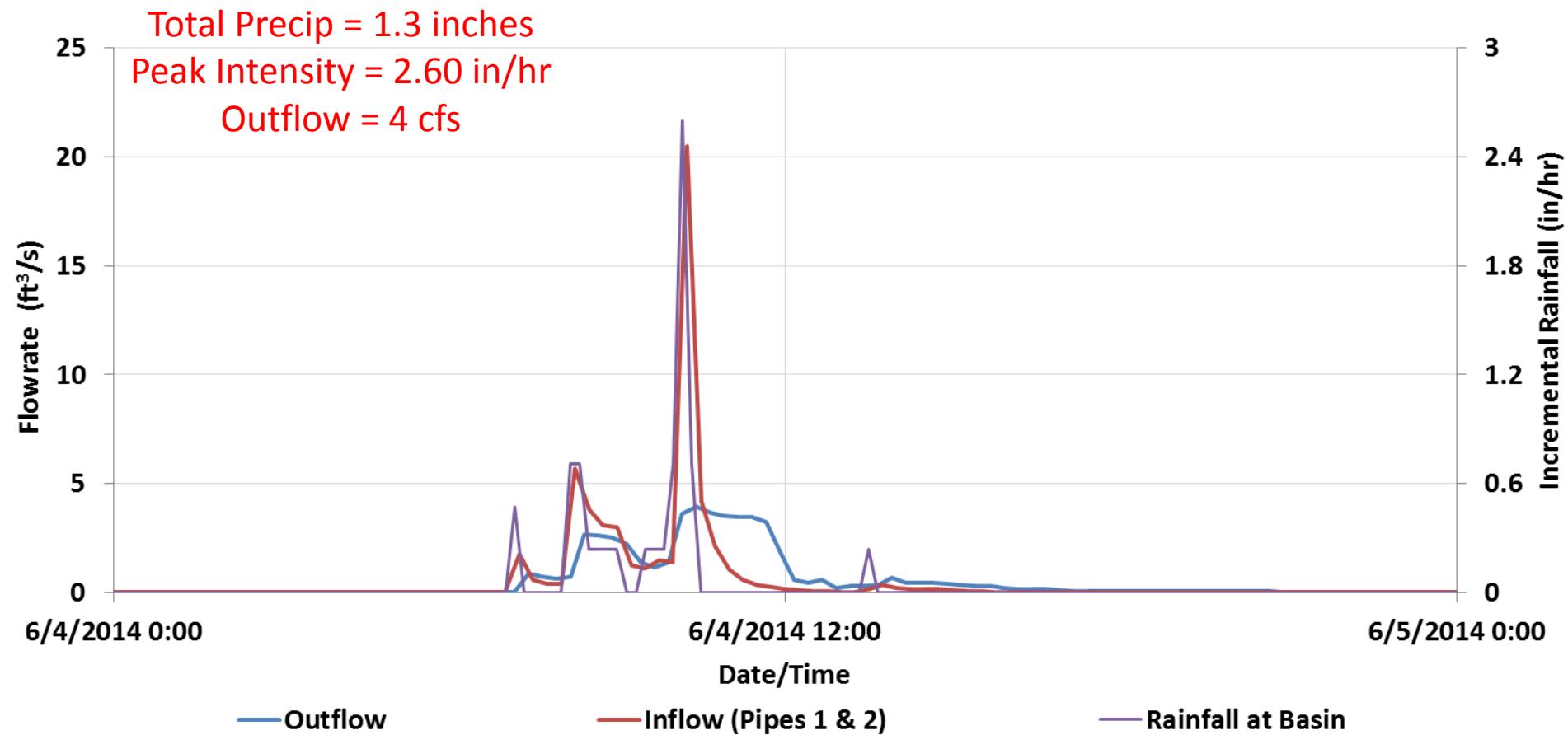
Post-retrofit outflow:

All design storms < pre-retrofit outflow

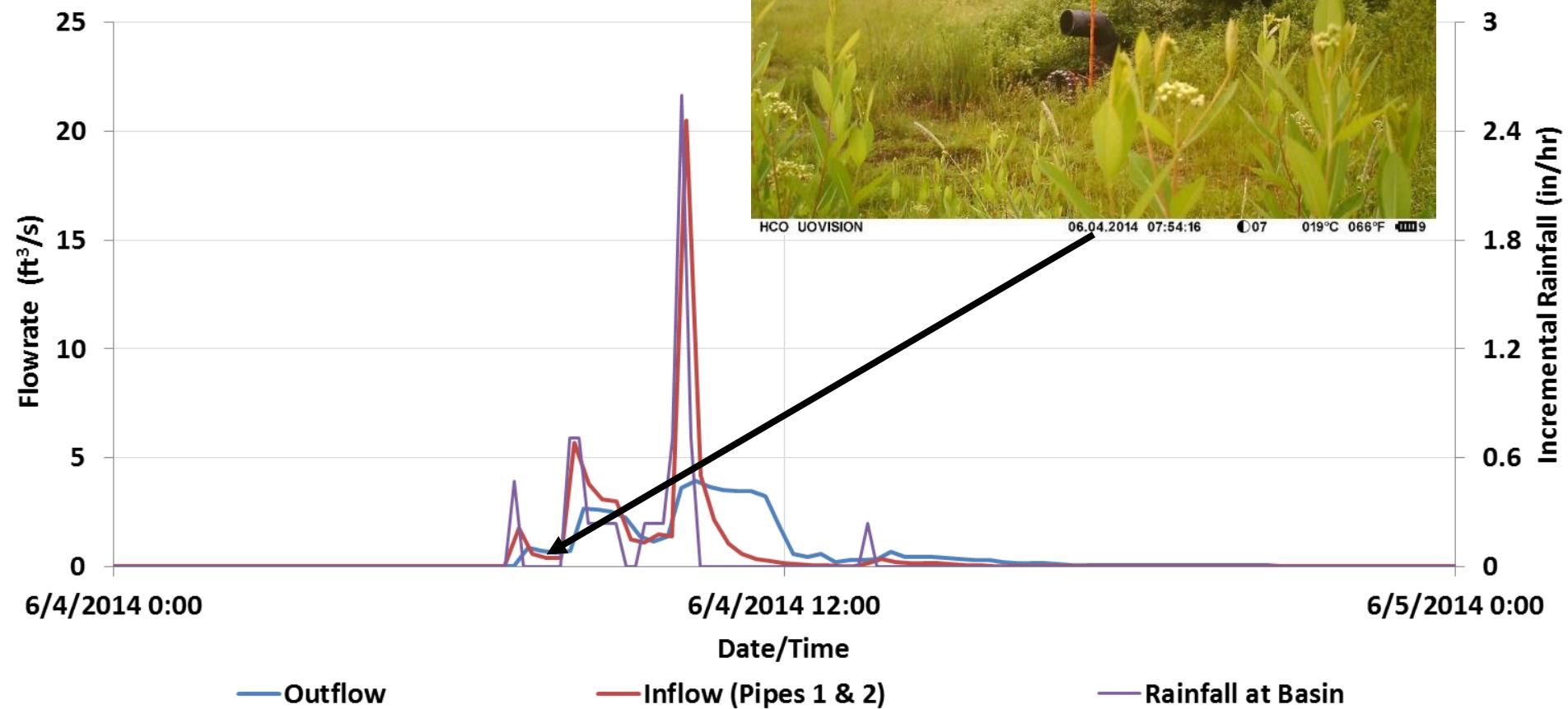
1-yr and 2-yr storms < $Q_{critical}$ (20.6 cfs)

Detention Basin Retrofit

Post-installation Monitoring

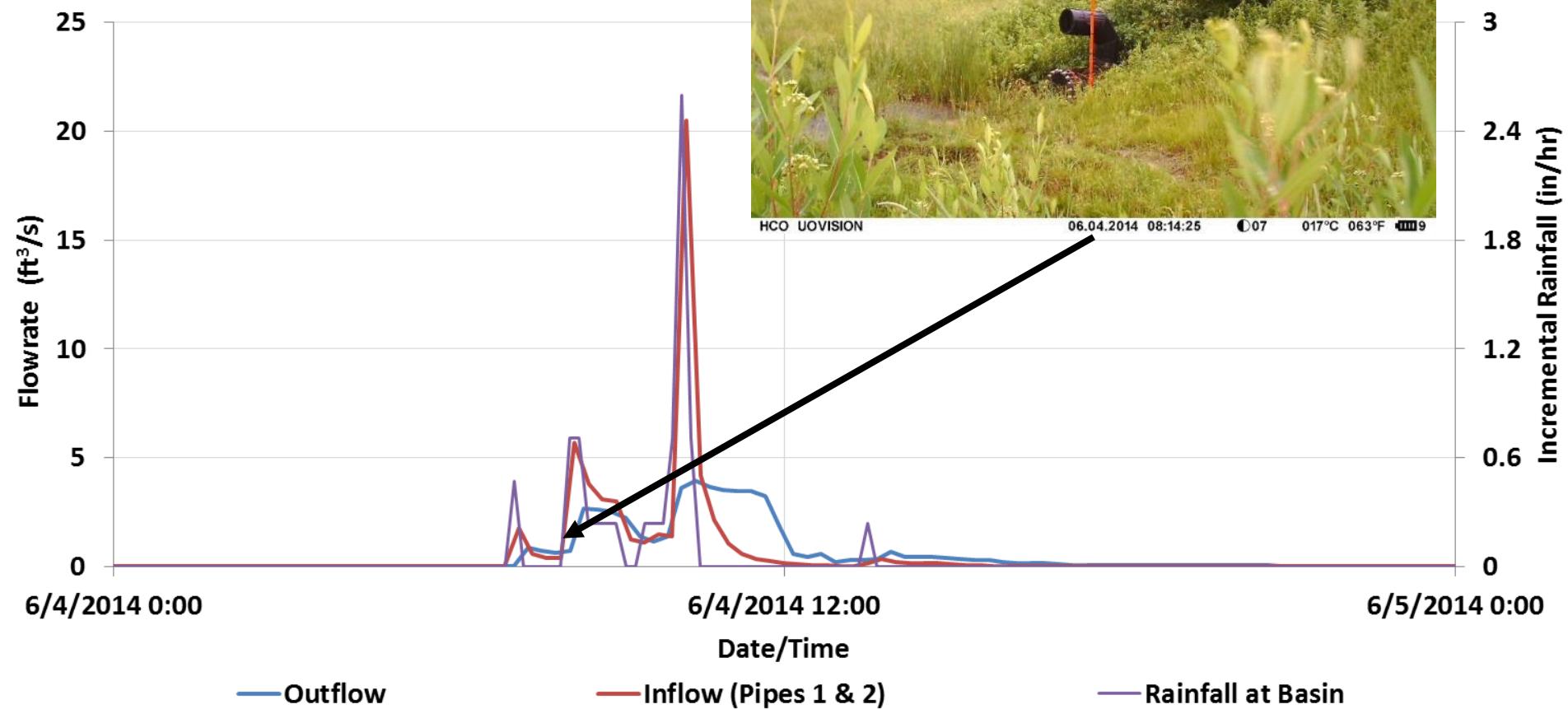


Post-retrofit

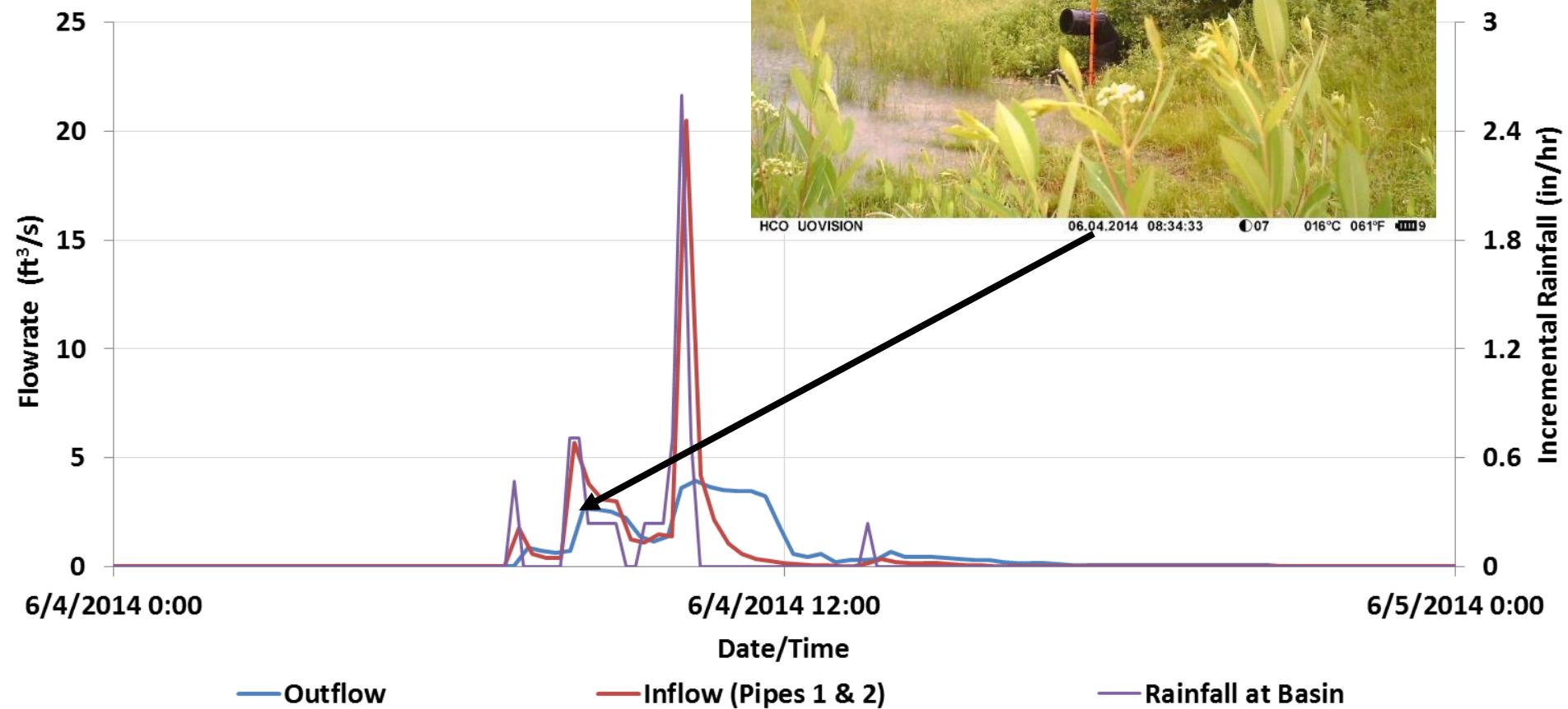


Adapted from Hawley et al. (In review)

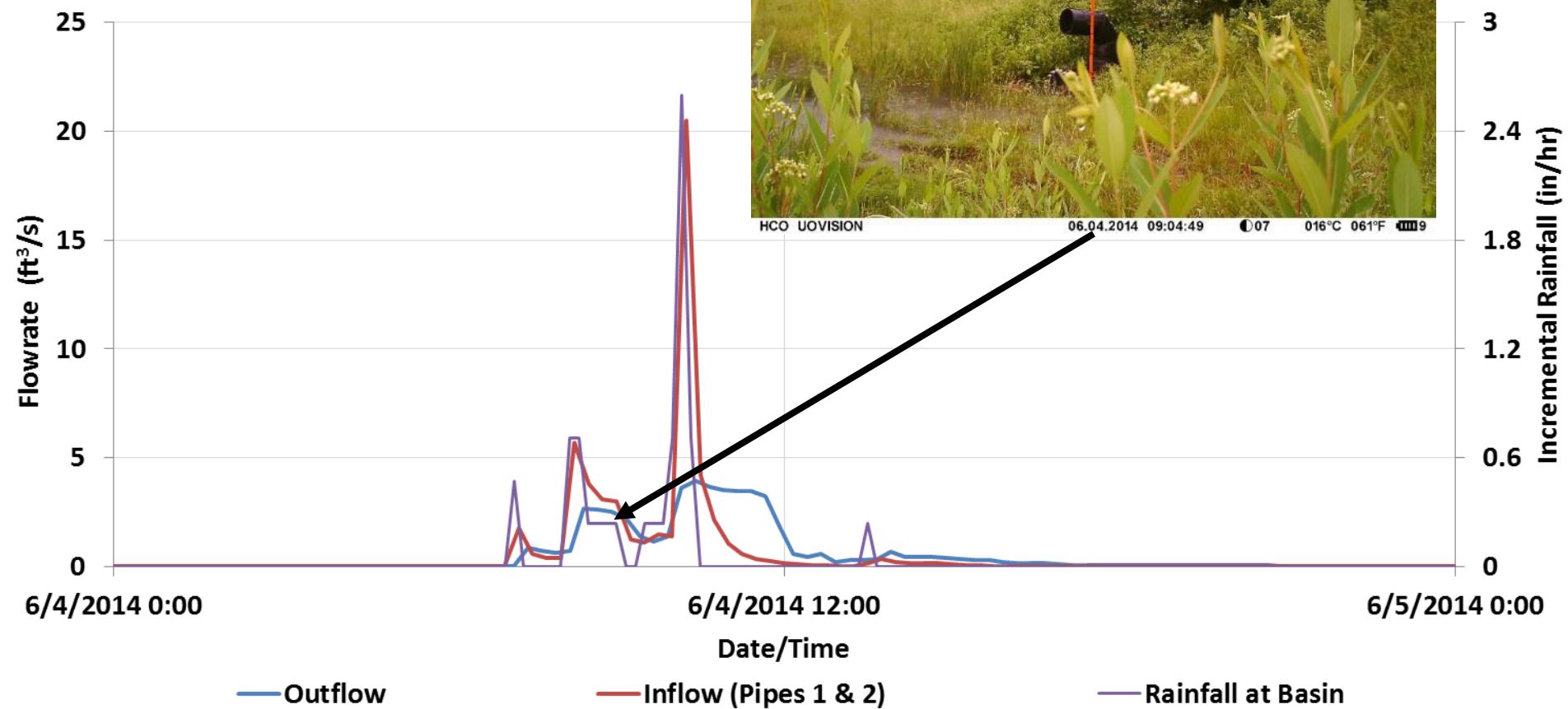
Post-retrofit



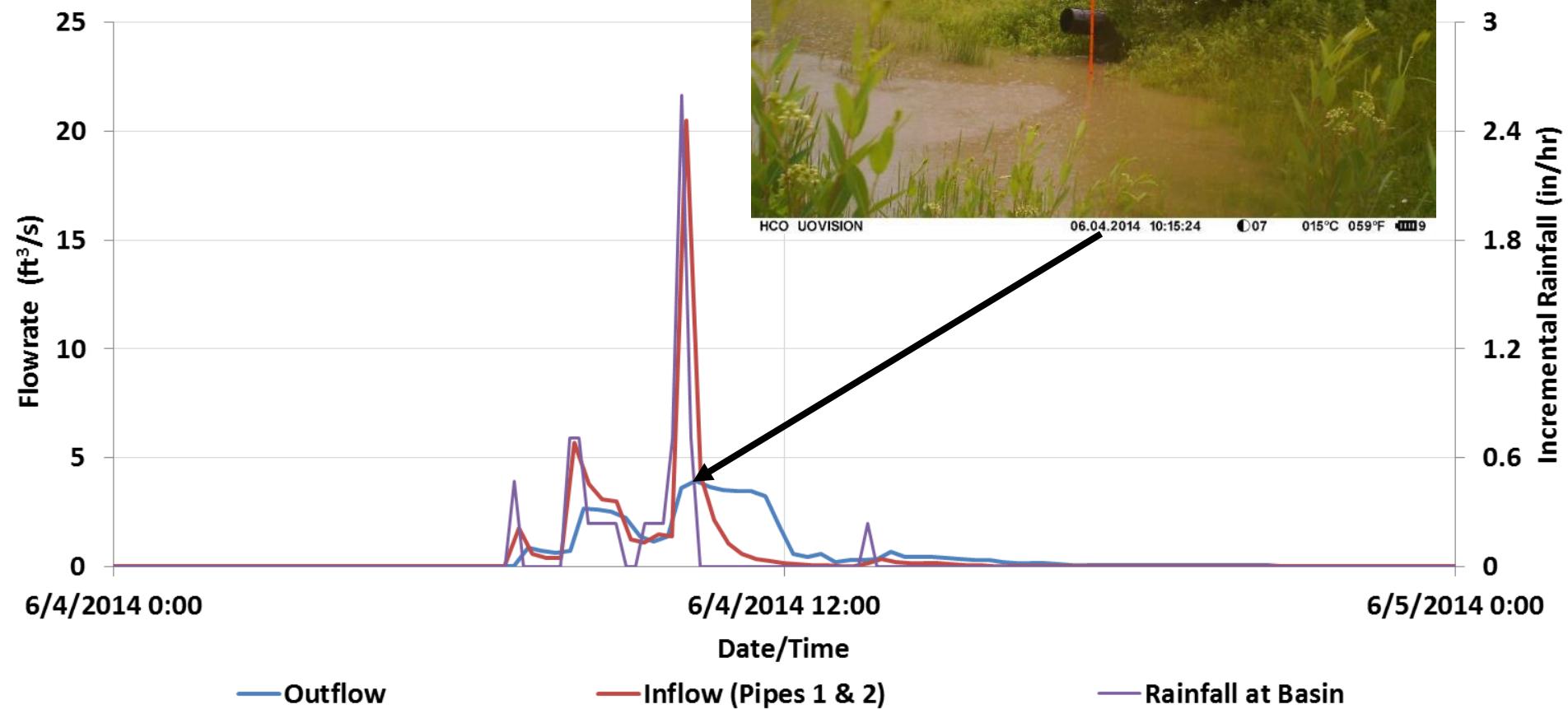
Post-retrofit



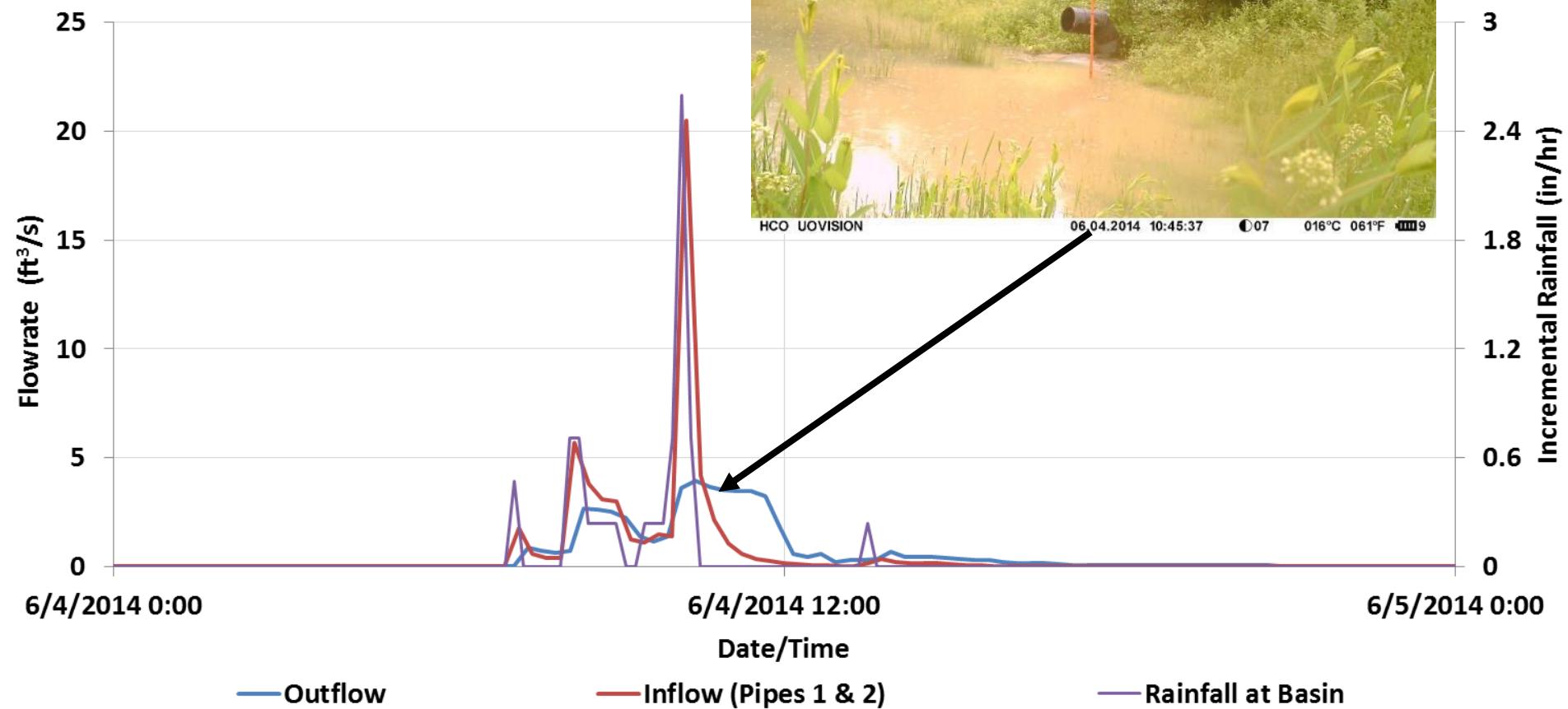
Post-retrofit



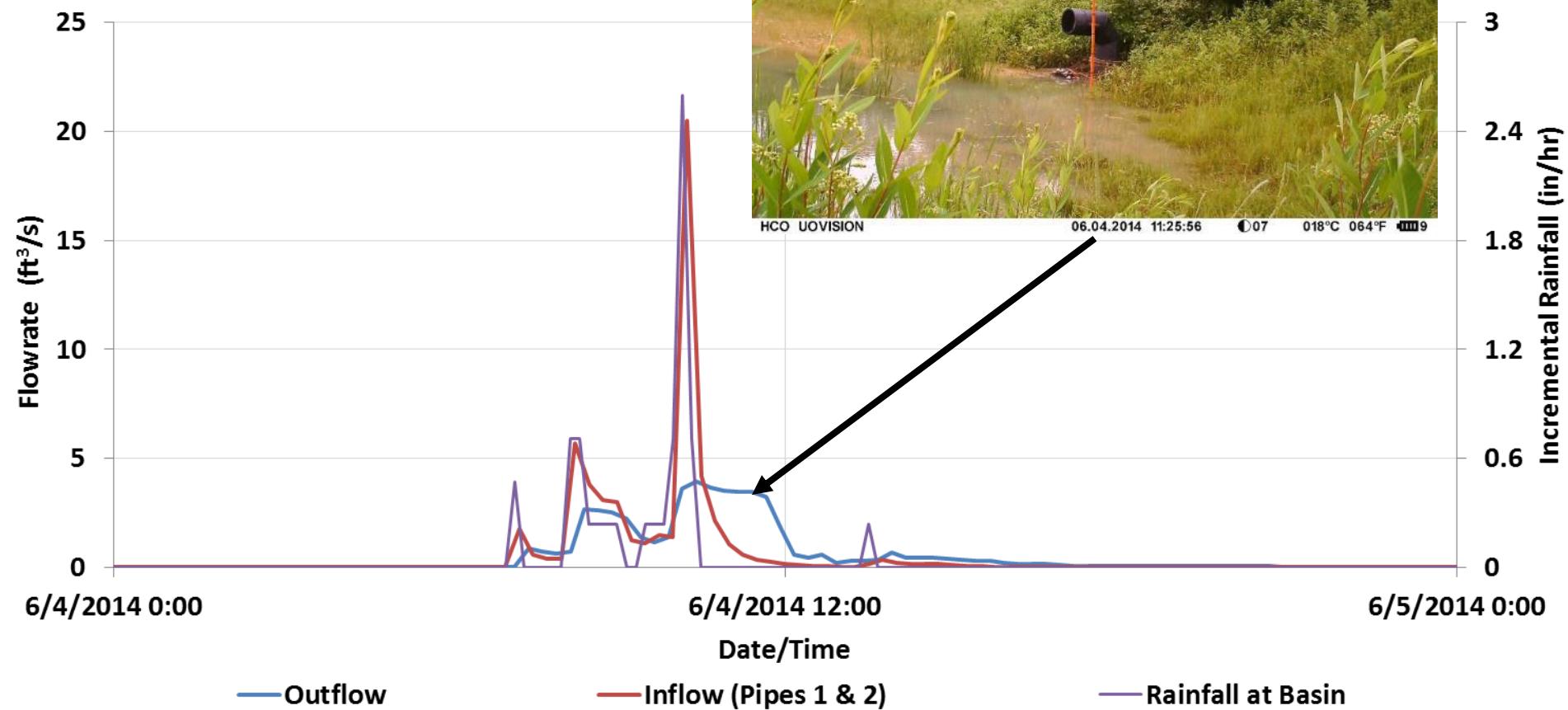
Post-retrofit



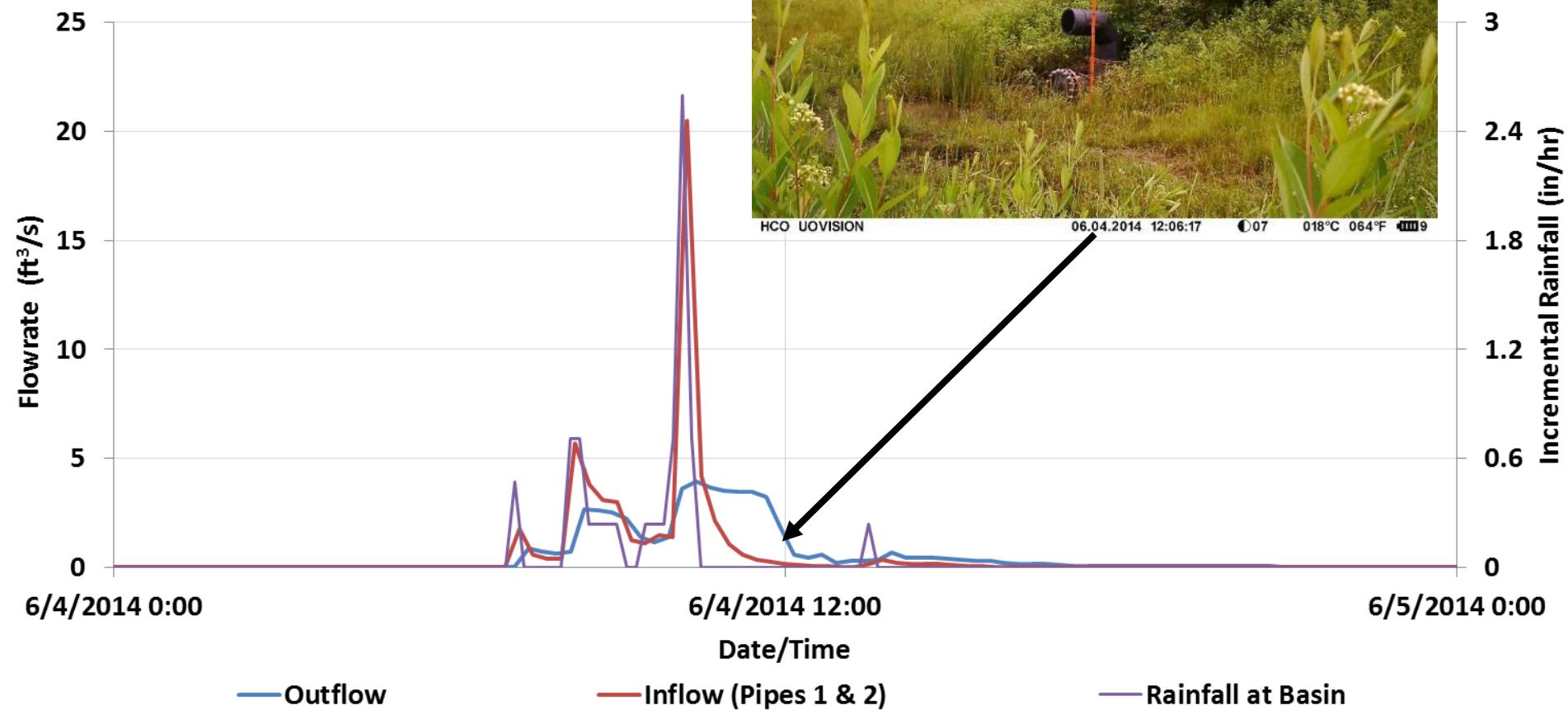
Post-retrofit



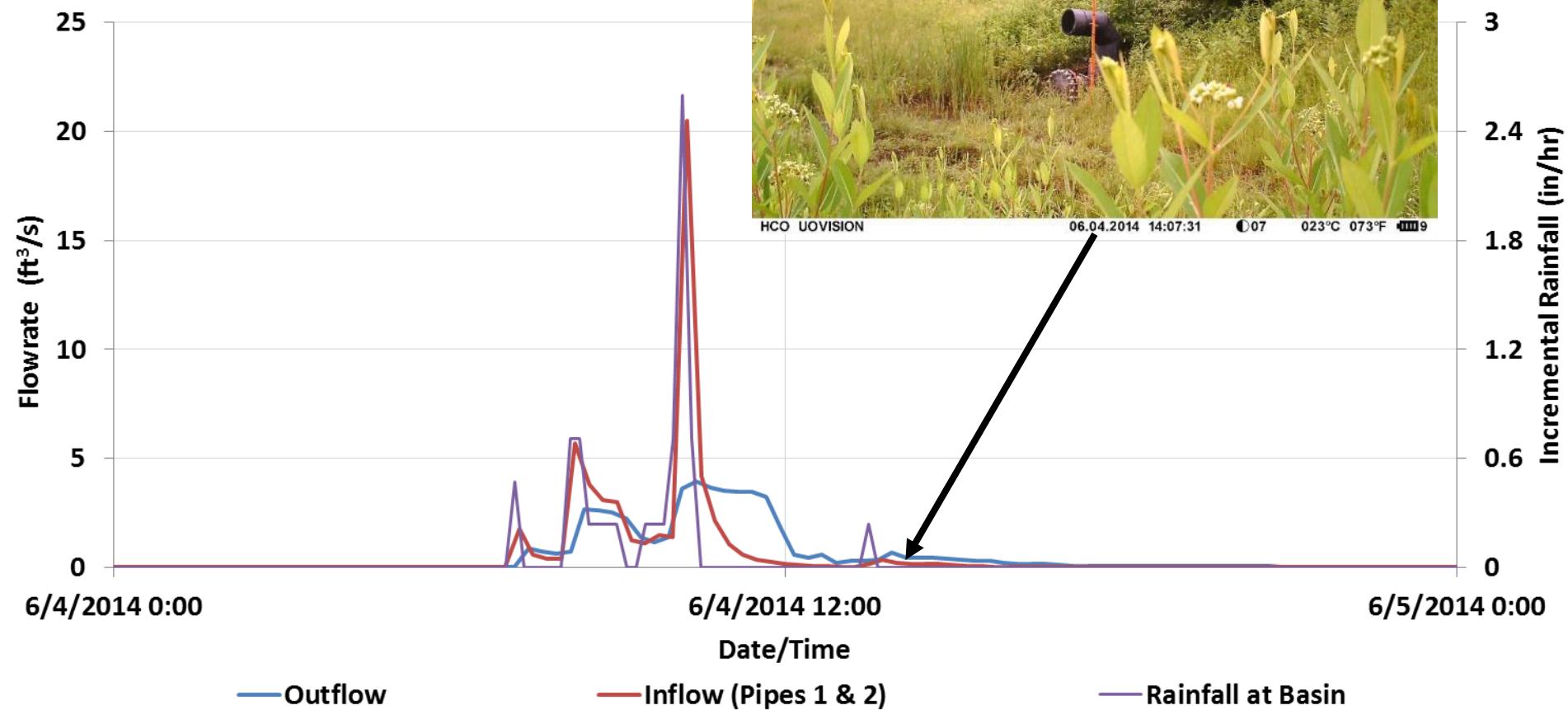
Post-retrofit



Post-retrofit



Post-retrofit

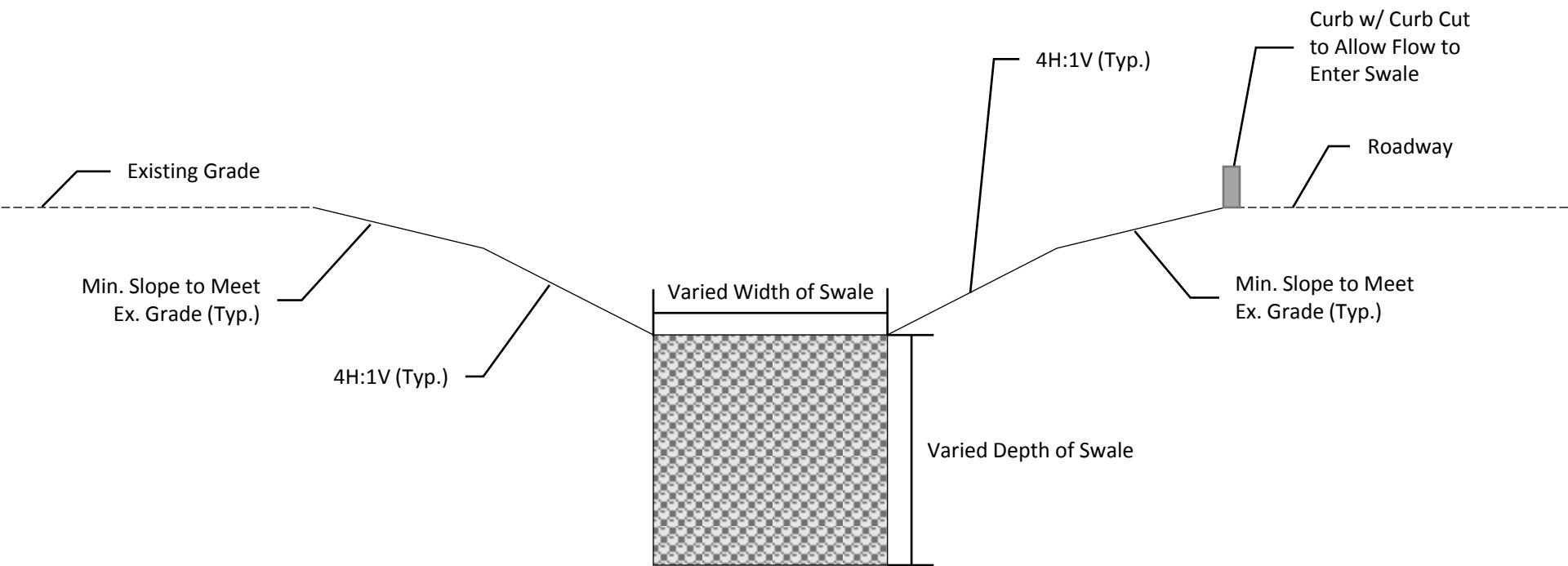


Example 3

Enhanced Swale



Enhanced Swale Cross Section

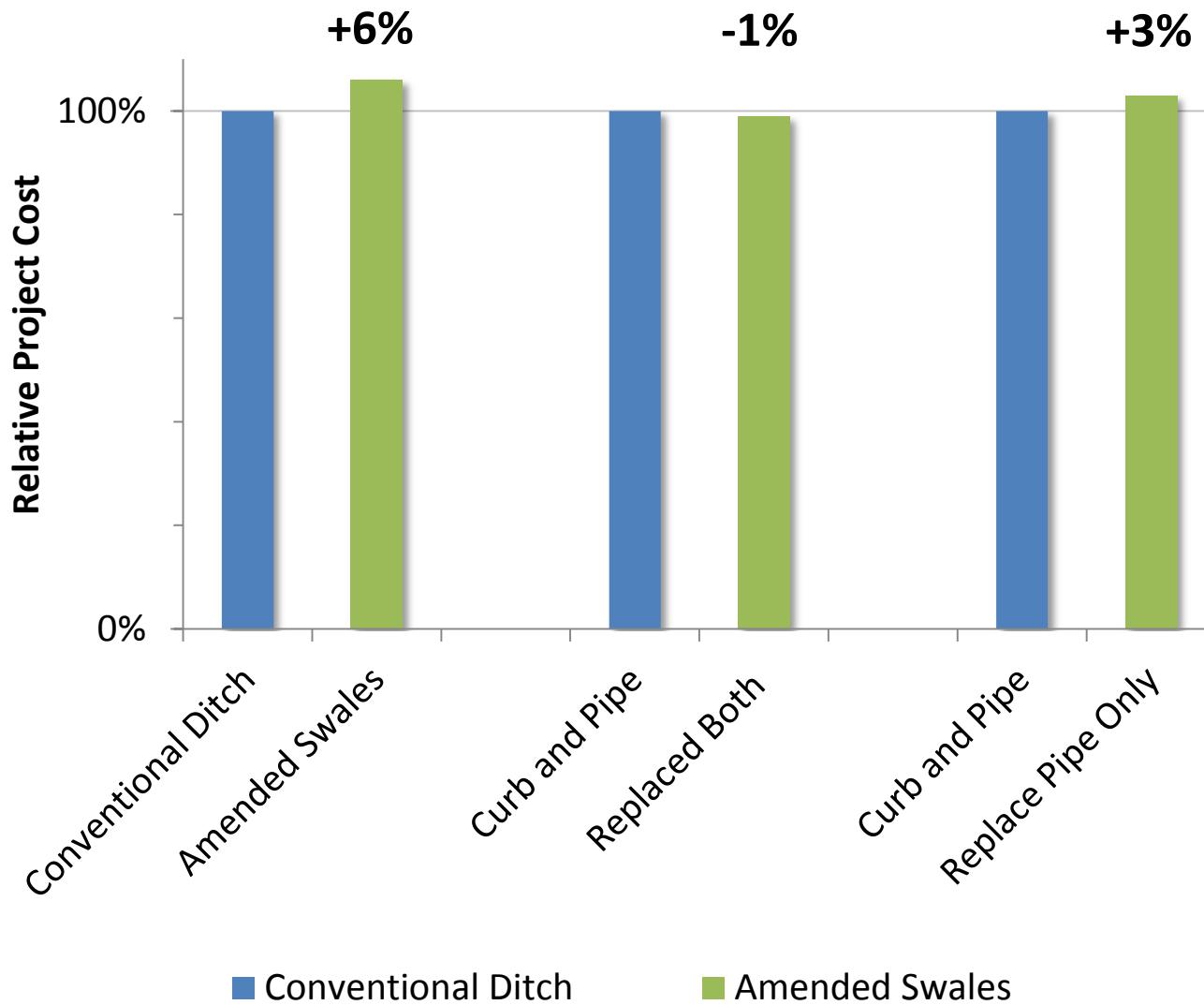


Enhanced Swale Components

- Gravel
 - Sized to resist erosion
 - Steep slopes: rip rap
 - Gentle slopes: gravels
- Other variations have included:
 - Topsoil
 - Vegetation
 - Turf grass or natives depending on preference



Preliminary Costs



Example: Enhanced Swale Preliminary Results

Swale/ Roadway	Drainage Area <i>acres</i>	Pre Q ₂ <i>cfs</i>	Q _{critical} (44% Q ₂) <i>cfs</i>	Post Q ₂ <i>cfs</i>	Post Q ₂ Control <i>cfs</i>	Swale Length <i>ft</i>	Bottom Width <i>ft</i>	Gravel Depth <i>ft</i>	Gravel Volume <i>CY</i>
Veterans Way									
1	0.35	0.81	0.36	1.10	0.31	213	14	2	70.7
2	0.46	0.84	0.37	1.48	0.33	132	14.25	5	111.84
3	0.80	1.30	0.57	2.67	0.52	541	10	3.1	198.8
4	0.19	0.31	0.14	0.64	0.14	54	27	3	51.8
North Bend Road									
5	2.15	5.50	2.42	7.90	1.63	956	8.6	3.1	301.9
6	2.06	3.75	1.65	7.60	1.30	810	14	4.1	550.9
Burlington Pike									
7	2.11	4.91	2.16	8.22	1.66	451	15	6.25	501.4
8	1.74	4.26	1.87	6.79	1.46	376	15.25	5	339.6

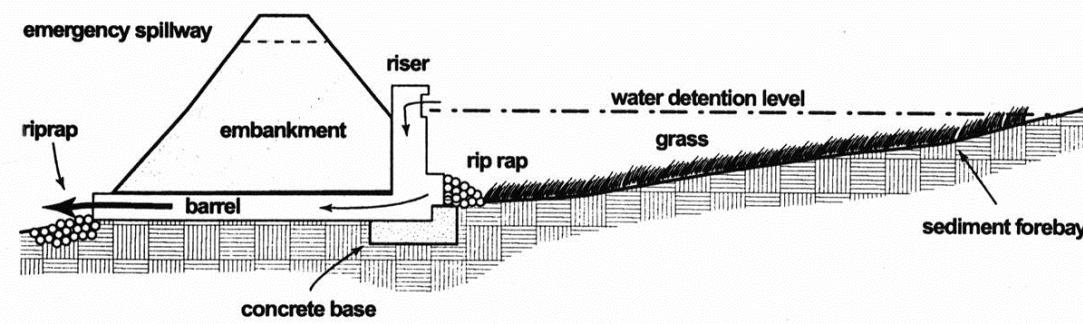
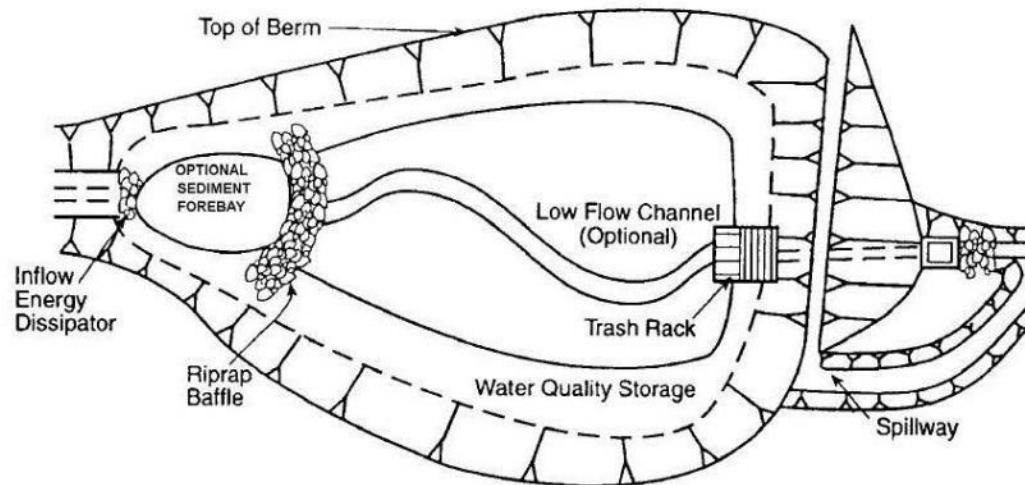
- ✓ Post ≤ Pre: 2-yr, 10-yr, 25-yr, 50-yr, 100-yr
- ✓ Water Quality Volume treated
- ✓ Q_{critical} controlled for 2-yr, 24-hr storm

Example 4

Extended Detention Basin



Extended Detention Basins



Example: Extended Detention

$$Q_{\text{critical}} = 0.4 * 17.89 \text{ cfs} = 7.16 \text{ cfs}$$

Event	Method	Pre-development cfs	Post-development No Control cfs	Post-development Flood Control & WQ cfs	Post-development Flood, WQ, Q_{critical} cfs
WQ Event	Rational	0.87	1.41	0.37	0.54
3-mo, 24-hr	SCS Type II	2.56	13.67	0.32	0.42
6-mo, 24-hr	SCS Type II	6.37	21.10	1.03	0.76
1-yr, 24-hr	SCS Type II	11.76	29.85	5.99	3.53
2-yr, 24-hr	SCS Type II	17.89	39.15	14.74	7.15
10-yr, 24-hr	SCS Type II	36.59	64.71	33.67	32.94
25-yr, 24-hr	SCS Type II	48.86	80.28	44.91	47.72
50-yr, 24-hr	SCS Type II	58.97	92.70	52.08	56.10
100-yr, 24-hr	SCS Type II	69.78	105.68	61.08	67.97

- Footprint Sizing:
 - Flood control and WQ only = 10,903 SF
 - Flood control, WQ, and Q_{critical} = 10,903 SF
 - Additional Design Time for optimization: 45 minutes

Resources



◊ About us ◊ Resources ◊ News ◊ Contact



◊ Science ◊ Service ◊ Solutions

Resources and Links

Peer-reviewed Journal Articles on Hydromodification:

Hawley, R.J. and B.P. Bledsoe. 2011. How do flow peaks and durations change in suburbanizing semi-arid watersheds? A southern California case study. *Journal of Hydrology* 405 (1-2), 69-82. [Read article »](#)

Hawley, R.J. and B.P. Bledsoe. 2013. Channel enlargement in semi-arid suburbanizing watersheds: A Southern California case study. *Journal of Hydrology*, 496: 17-30. [Read article »](#)

Hawley, R.J., Bledsoe, B.P., Stein, E.D., and B.E. Haines. 2012. Channel evolution model of semiarid stream response to urban-induced hydromodification. *Journal of the American Water Resources Association*, 48(4): 722-744. [Read article »](#)

Hawley, R.J., MacMannis, K.R., and M.S. Wooten. 2013. Bed coarsening, riffle shortening, and channel enlargement in urbanizing watersheds, northern Kentucky, USA. *Geomorphology* 201: 111-126. [Read article »](#)

Peer-reviewed Journal Articles on Hydromodification Management Approaches and Case Studies

Bledsoe, B.P., Stein, E.D., **Hawley, R.J.**, and D.B. Booth. 2012. Framework and tool for rapid assessment of stream susceptibility to hydromodification. *Journal of the American Water Resources Association*, 48(4): 788-808. [Read article »](#)

Hawley, R.J., Wooten, M.S., Vatter, B.C., Onderak, E., Lachniet, M.J., Schade, T., Grant, G., Groh, B., and J. DelVerne. 2012. Integrating stormwater controls designed for channel protection, water quality, and inflow/infiltration mitigation in two pilot watersheds to restore a natural flow regime in urban streams. *Watershed Science Bulletin*, 3(1), 25-37. [Read article »](#)

Technical Reports and Tools for Monitoring, Screening, and Managing Hydromodification:

Bledsoe, B.P., **Hawley, R.J.**, Stein, E.D. and D.B. Booth. 2010. Hydromodification Screening Tools: Technical Basis for Development Regionally Calibrated Probabilistic Channel Susceptibility Assessment. Southern California Coastal Water Research Project (SCCWRP) Technical Report 607. Costa Mesa, CA. July, 2010. 42 pp. [Download article \(PDF\)](#)

Featured article

Two recent papers on the effects of hydromodification from different settings published in the *Journal of Hydrology* and *Geomorphology*.

Available online:

[Channel Enlargement in Southern California »](#)

[Riffle Shortening in Northern Kentucky »](#)

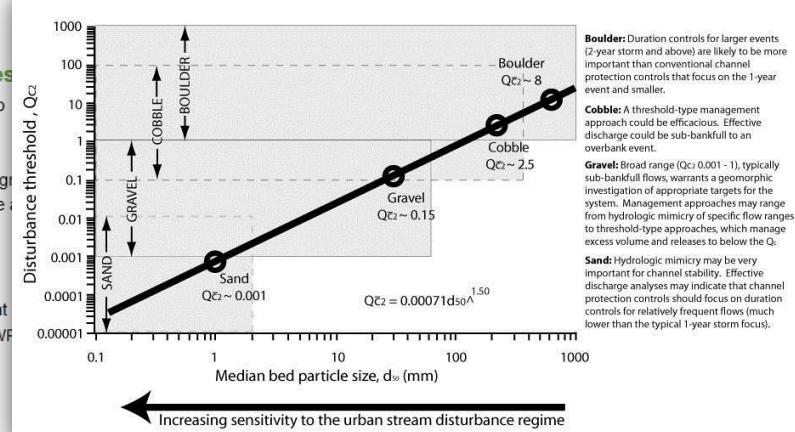


Matt Wooten

Aquatic Biologist, SD1

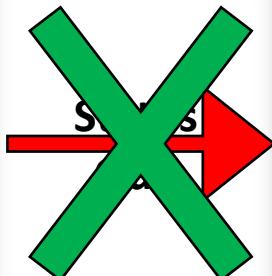
859-578-6887

mwooten@sd1.org



Adapted from Hawley and Vietz (In Press, *Freshwater Science*)

Find an Appropriate Approach for Your Community



1. Prevent Future Problems:

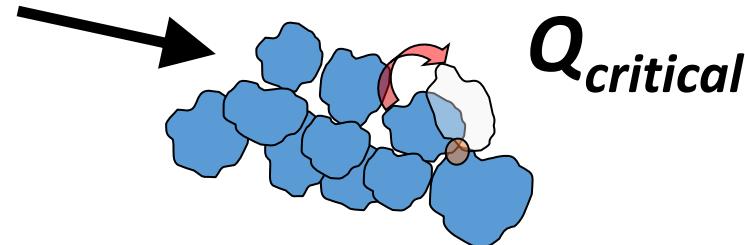
- Optimize Post Construction Rules & Regs to Protect Your Streams

2. Mitigate Existing Problems:

- Find Cost-effective Solutions to Mitigate Existing Impacts

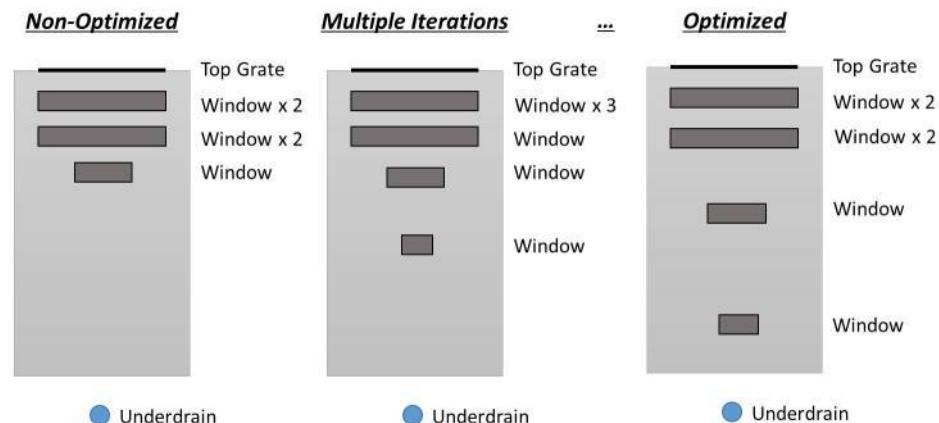
1. The $Q_{critical}$ Design Offers A Practical Approach to Rules & Regs in N.KY

- $Q_{critical}$ Design Target ~40% of Pre-developed Q_2



- Releasing 2-year storm below $Q_{critical}$ Achieves

- ✓ Similar Basin Sizes
- ✓ Similar Design Process
- ✓ Long-term Stability



2. Retrofitting Existing Detention Basins Offers A Cost-effective Approach to Mitigate Existing Impacts

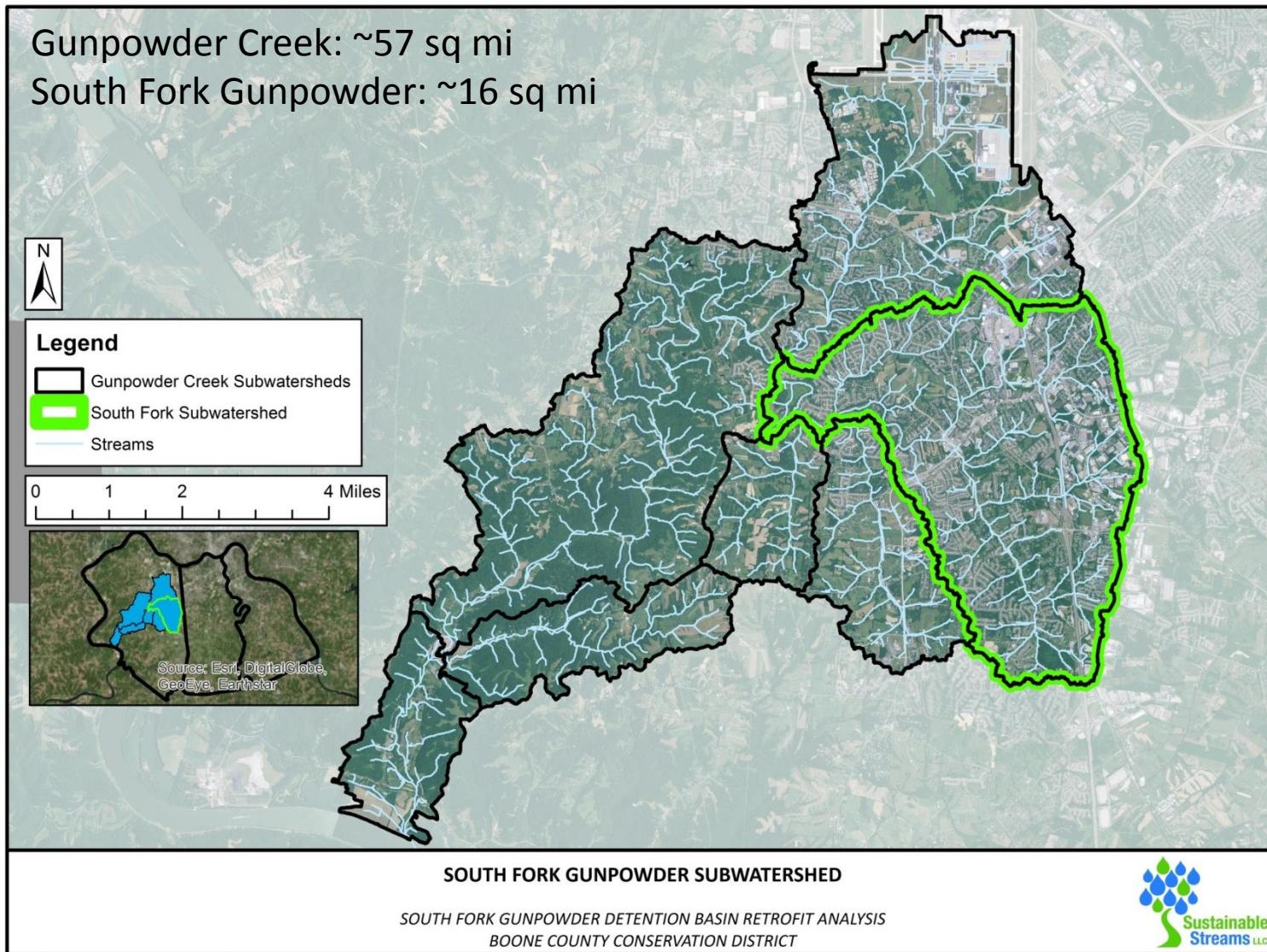
Strategy	Cost per Acre Treated	Notes
Distributed GI	~\$50,000	King Co. (2013) pilot study
Stream Restoration	~\$5,000	Equivalent of ~\$200-300 per foot
New Detention	~\$3,000	Hawley et al., 2012
Retrofit Detention	~\$500	“Kraken” (EPA, Patent Pending) \$10,000 installed by Site Supply



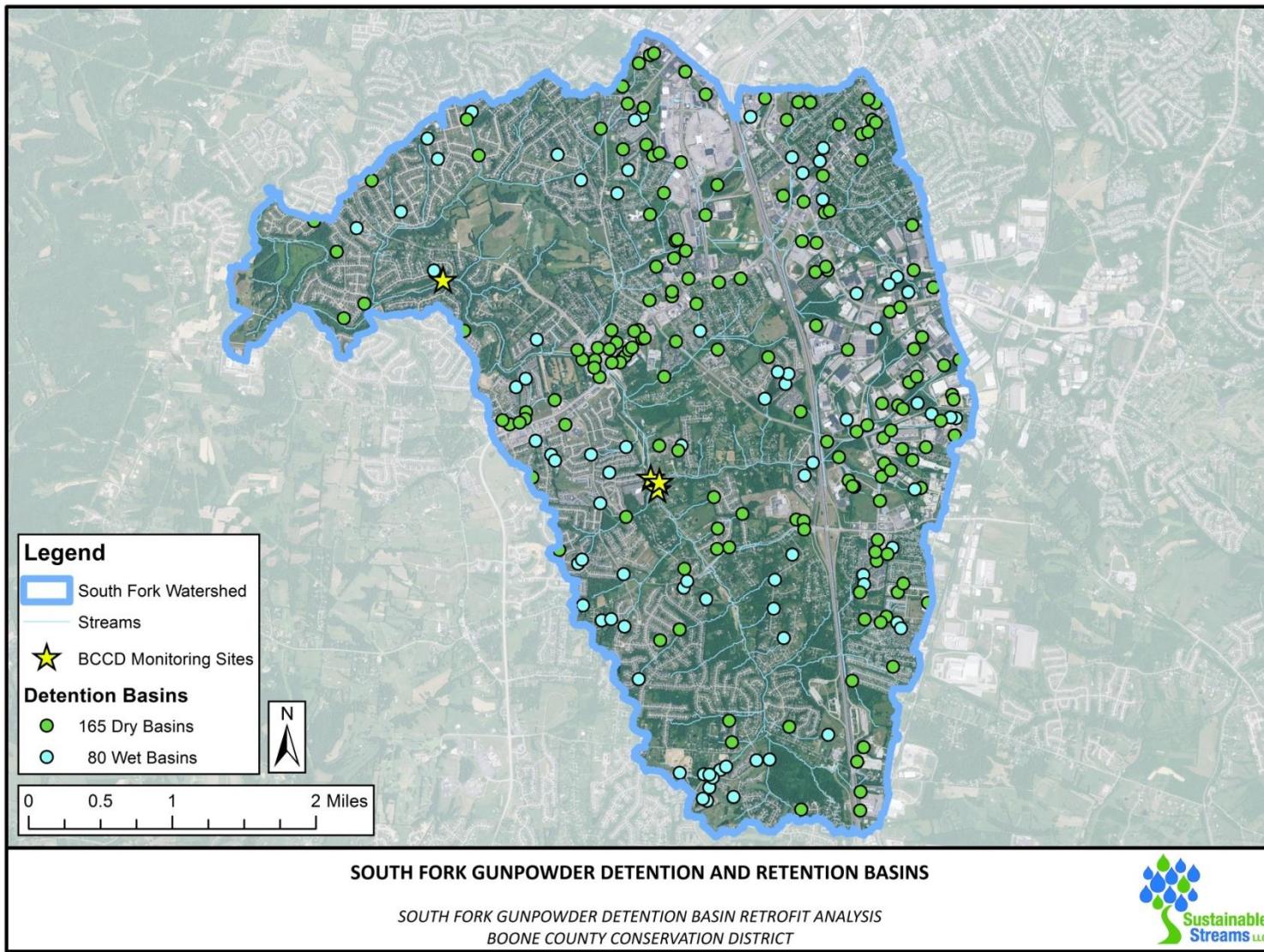
Adapted from Hawley et al. (In Review)

Watershed Planning Case Study

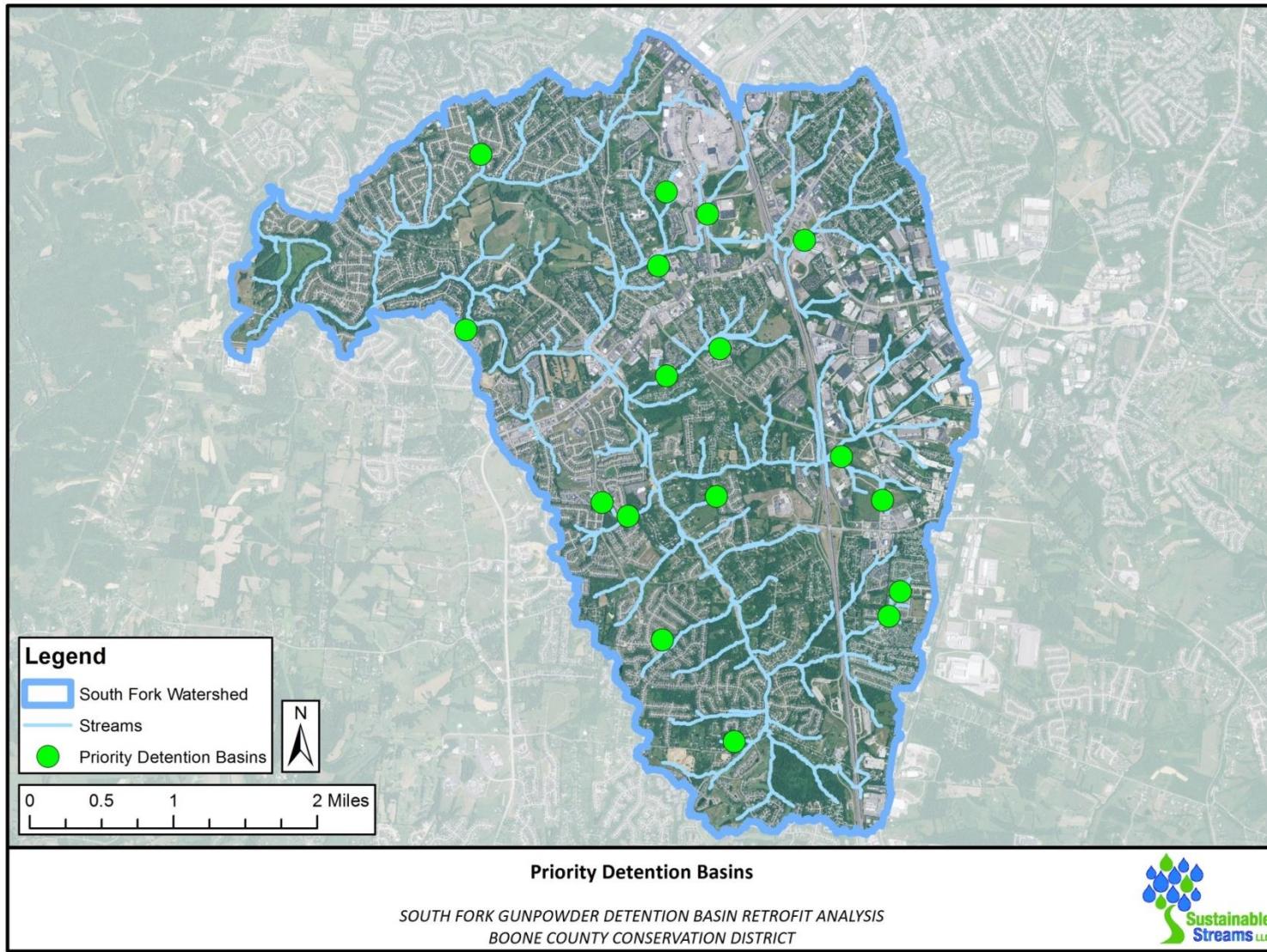
Combines Retrofits with Bankfull Wetlands



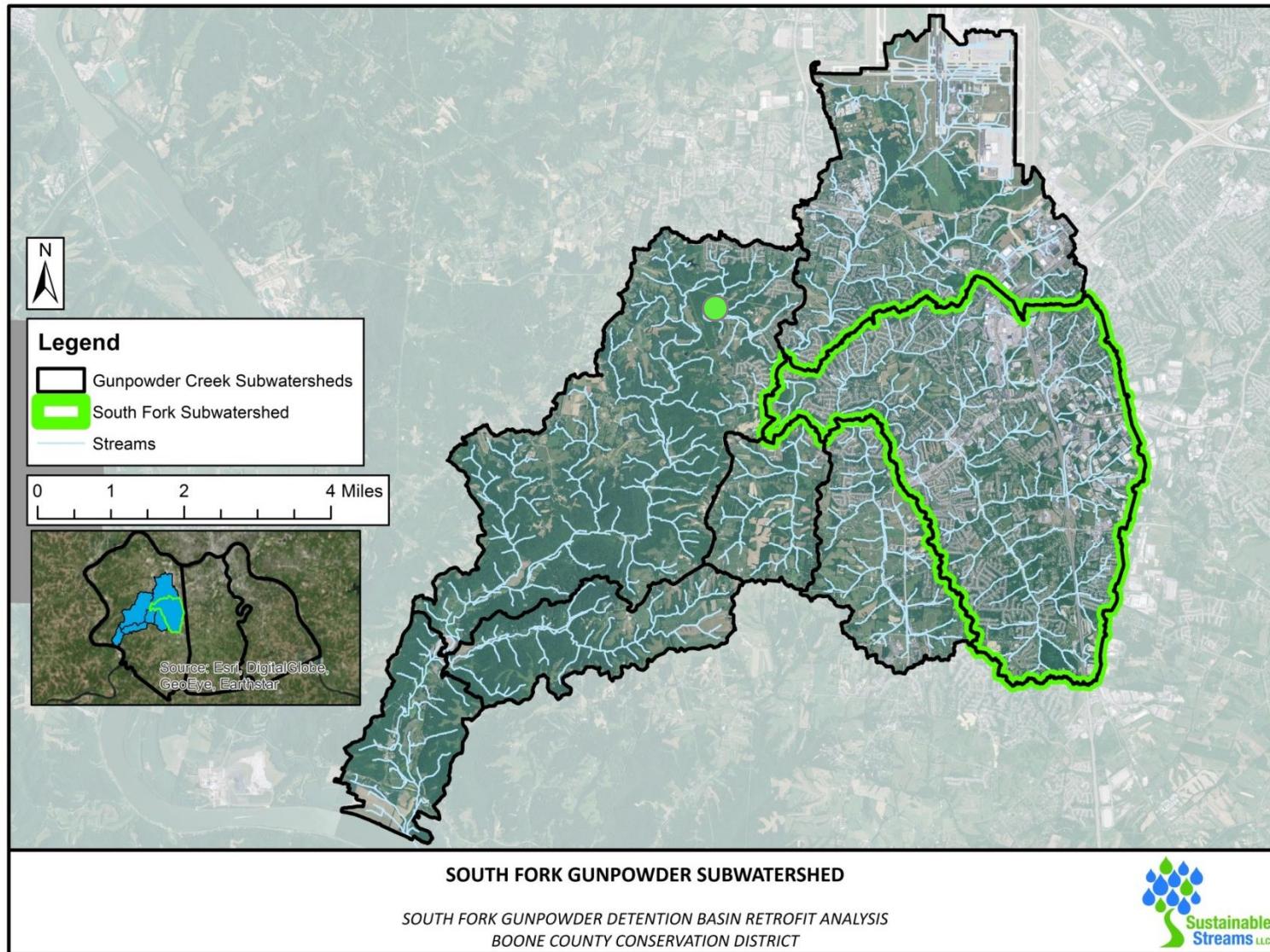
245 Existing Detention Basins Provide ~460 ac-ft of storage



17 Prioritized Basins for Retrofitting Can Optimize 94 ac-ft of storage (>20%)



Strategic Opportunities for New Storage Using Bankfull Wetlands



Proposed Bankfull Wetlands Increases Habitat and Reduces Q_{critical} Flows

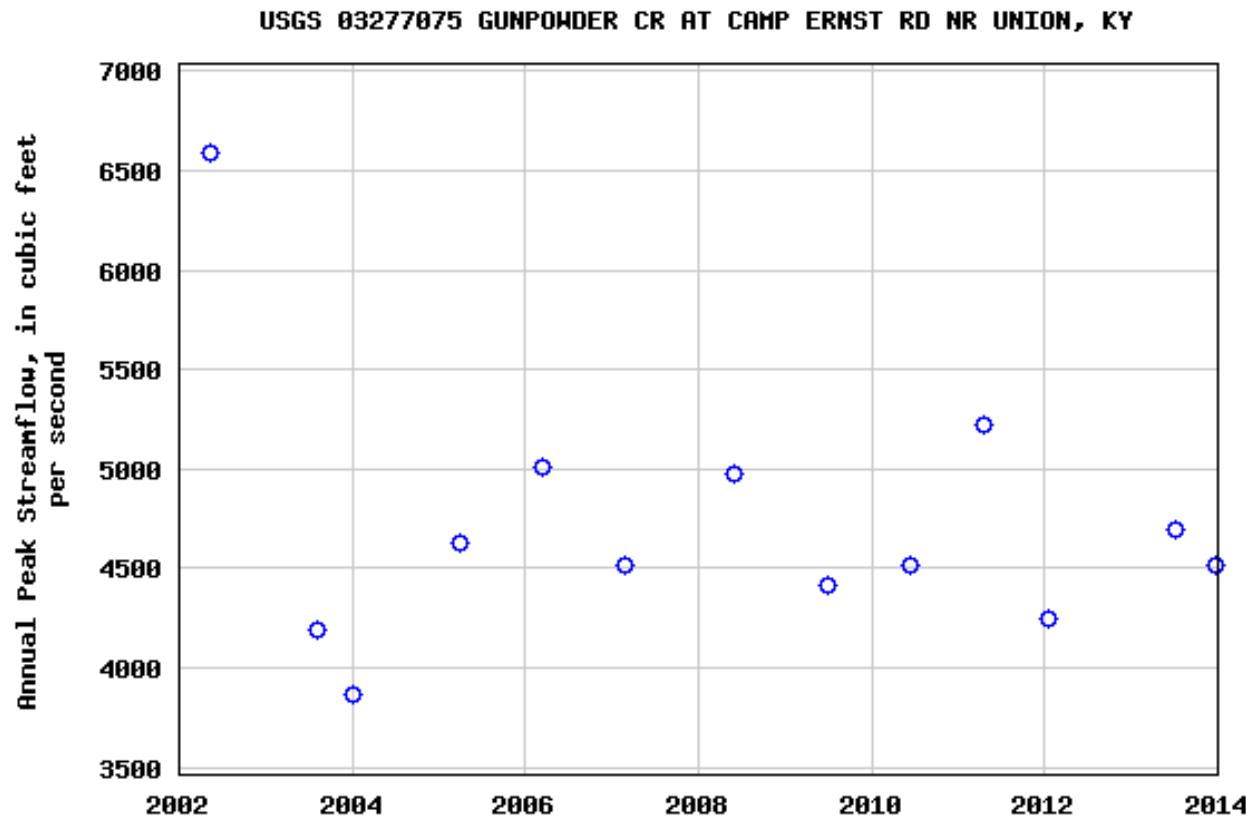


Creates Storage in a Previously Disconnected Floodplain



Qc estimated as 2000 cfs

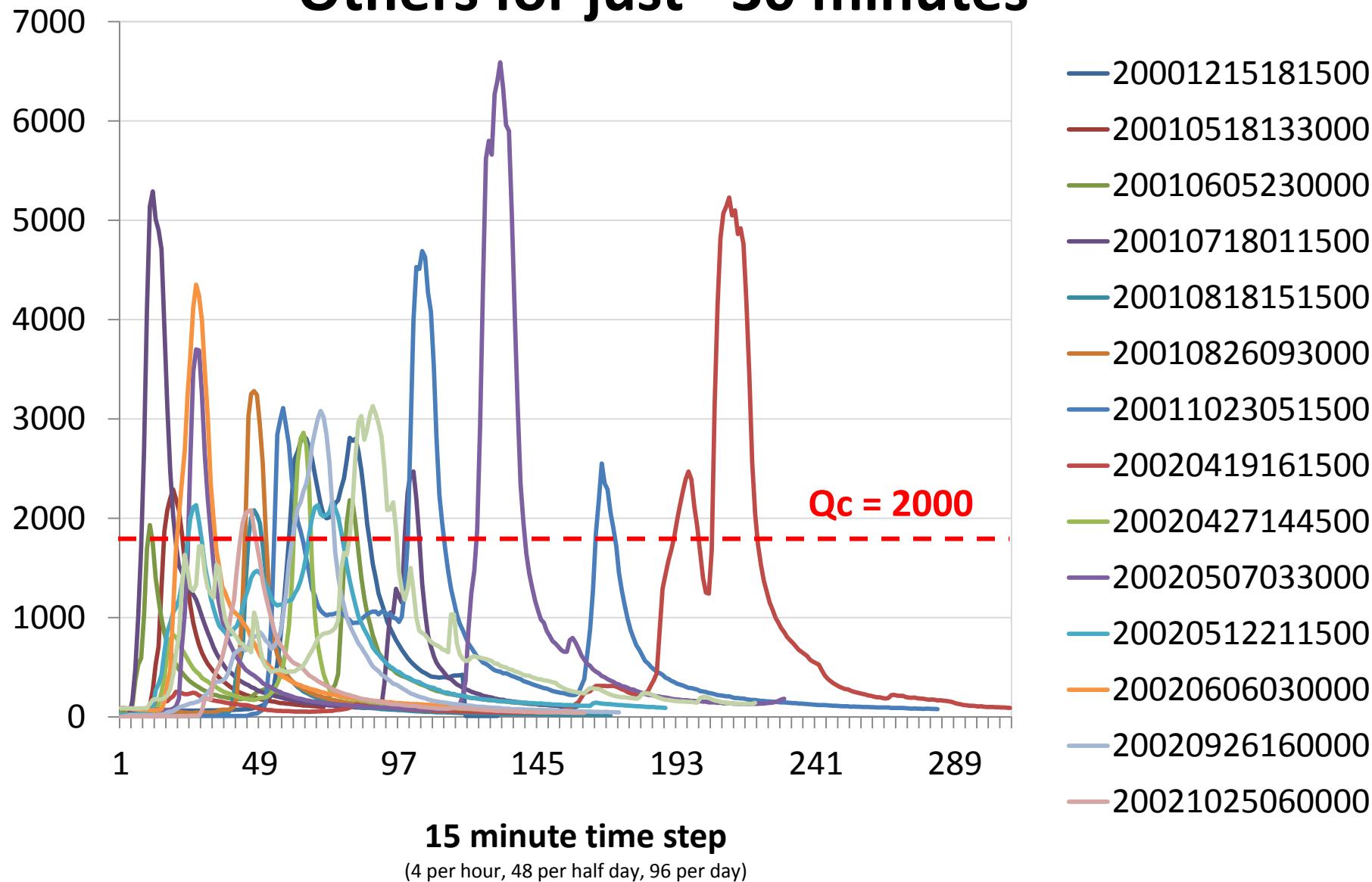
Gunpowder Creek Exceeds Qc Every Year



2001-2002 ~ 13 Events Exceeded Qc

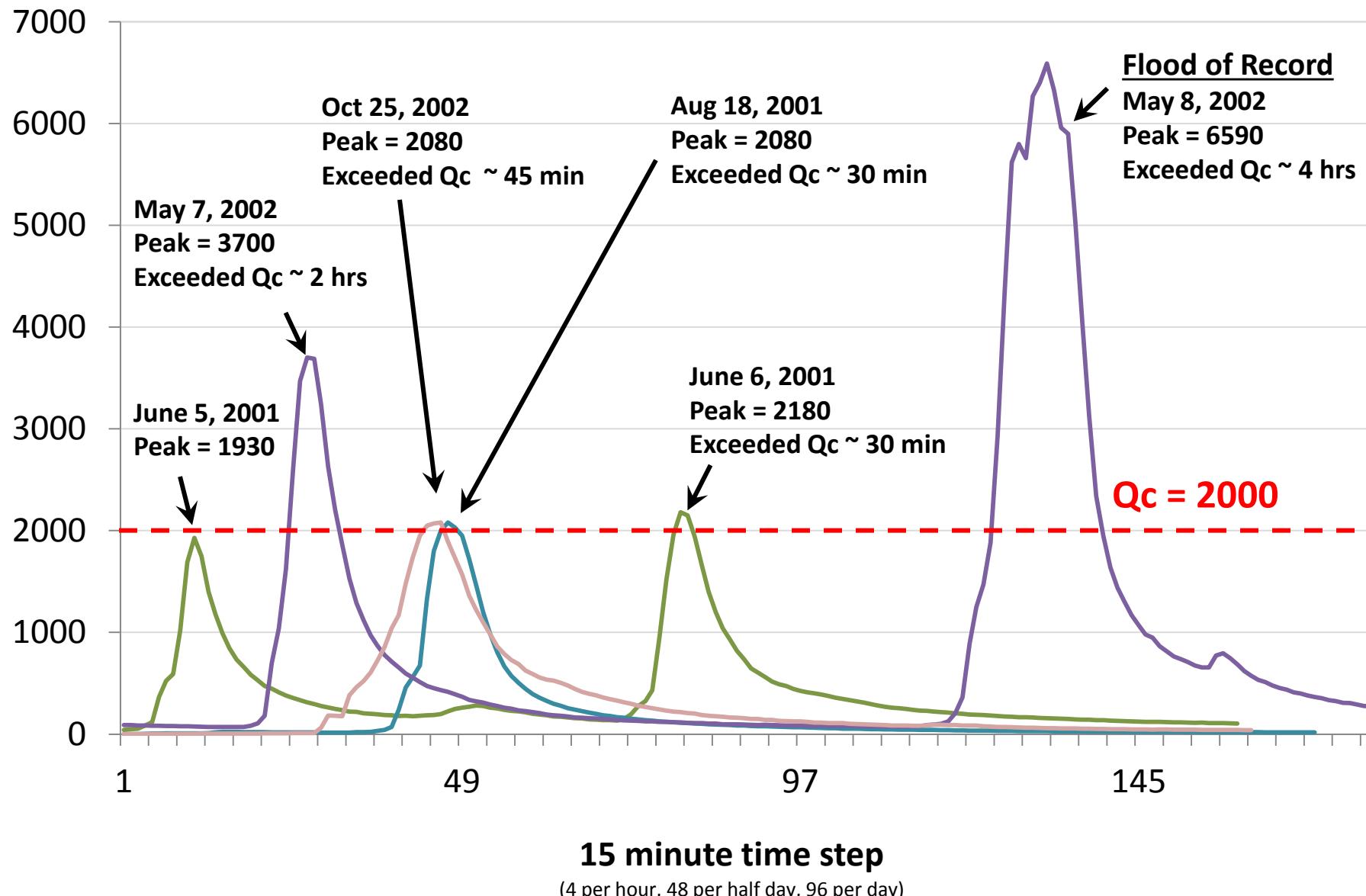
Some for up to ~ 12 hours

Others for just ~30 minutes



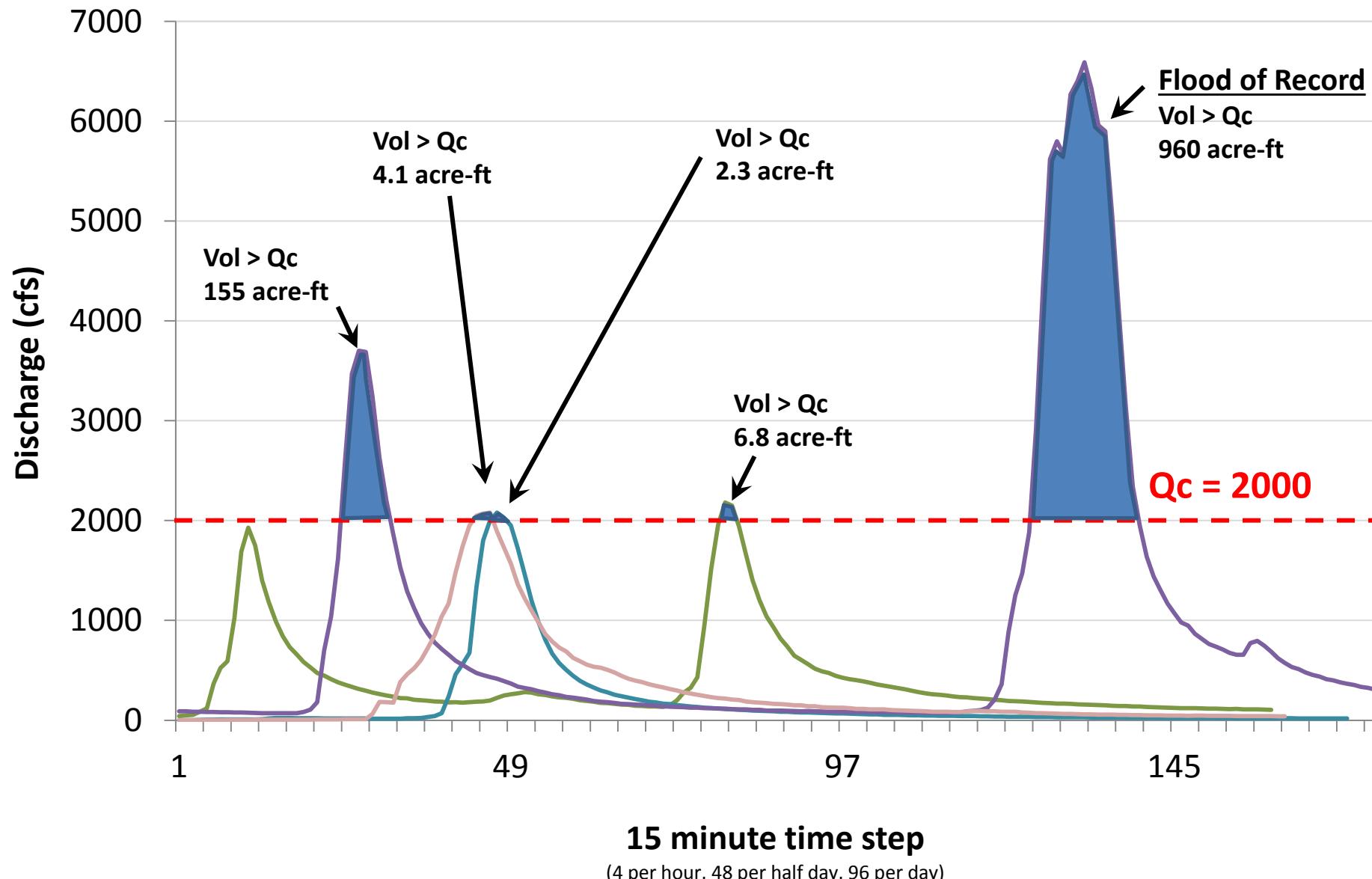
2001-2002

3 Out of the 13 Events Barely Exceed Qc

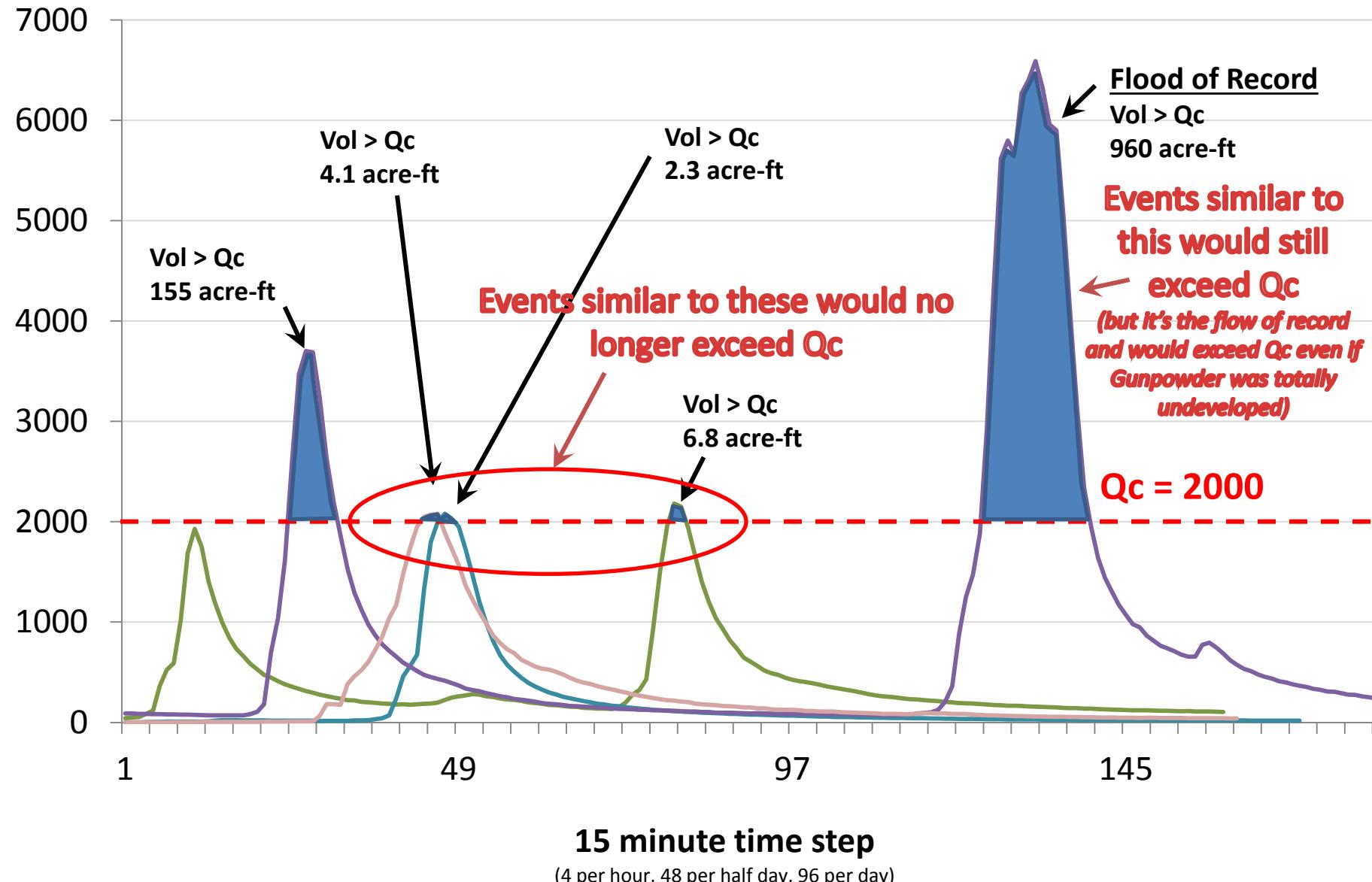


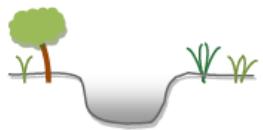
2001-2002

3 Out of the 13 Events Barely Exceed Qc

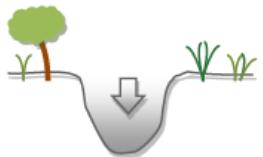


YMCA Bankfull Wetlands Will Store ~ 5-7 acre-ft above Qc





Stage 1 – Equilibrium



Stage 2 – Incision



Stage 3 – Widening



Stage 4 – Aggradation



Stage 5 – Equilibrium

Channel Evolution Sequence in Response to Increased Flows from Urbanization, Adapted from Schumm et al. (1984) and Hawley et al. (2012)



Conclusion

Successfully Managing Stream Stability:

- Protects Natural Resources
- Protects Infrastructure
- Protects Property

Biological

Physicochemical

Geomorphology

Hydraulics

Hydrologic

Stormwater Management

It all starts here



Thank You!



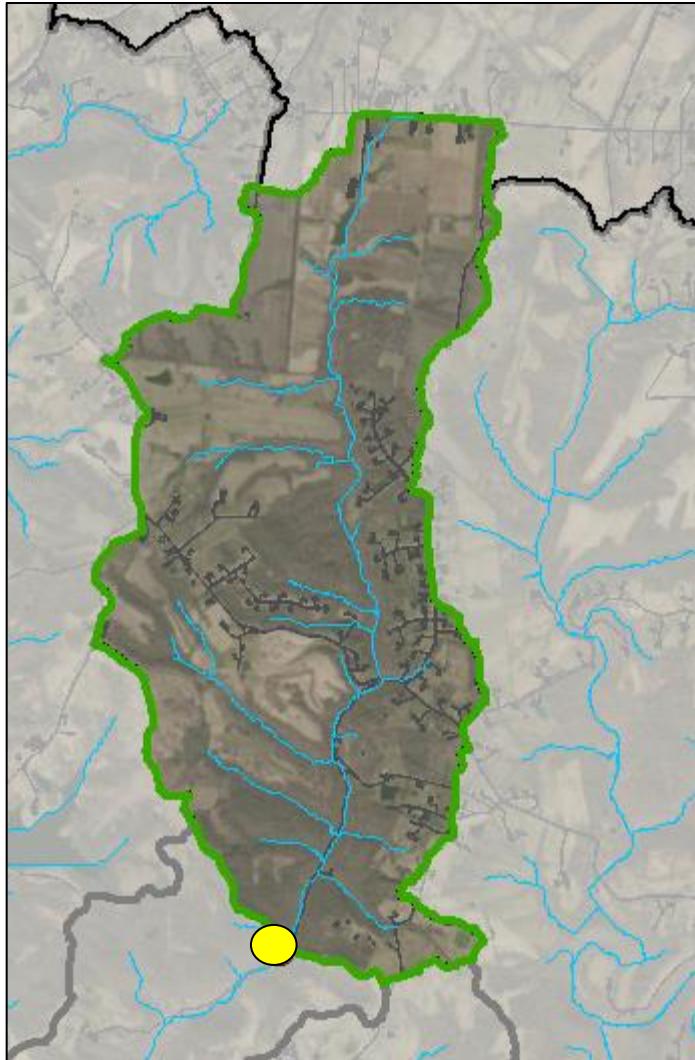
Photo by Mark Jacobs (Boone County Conservation District)



**Sustainable
Streams LLC**

Science · Service · Solutions

Stream Flow in Undeveloped Watershed



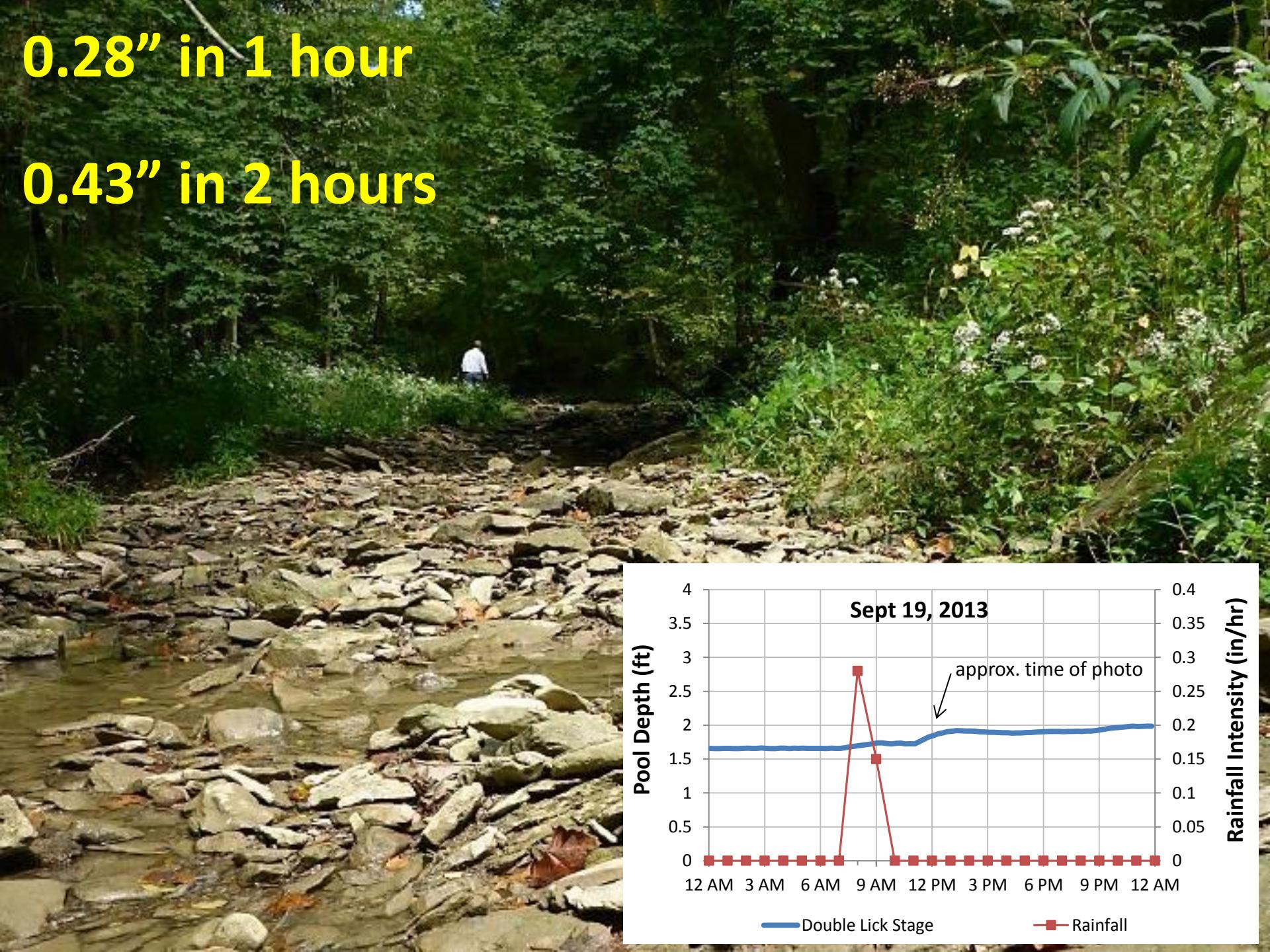
Double Lick Creek

1.8 square miles, 3% impervious

Outstanding State Resource Water

0.28" in 1 hour

0.43" in 2 hours



Stream Flow Downstream of Conventional Development



Sand Run
2.2 square miles, 29% impervious



Sand Run

08/28/2008 11:14

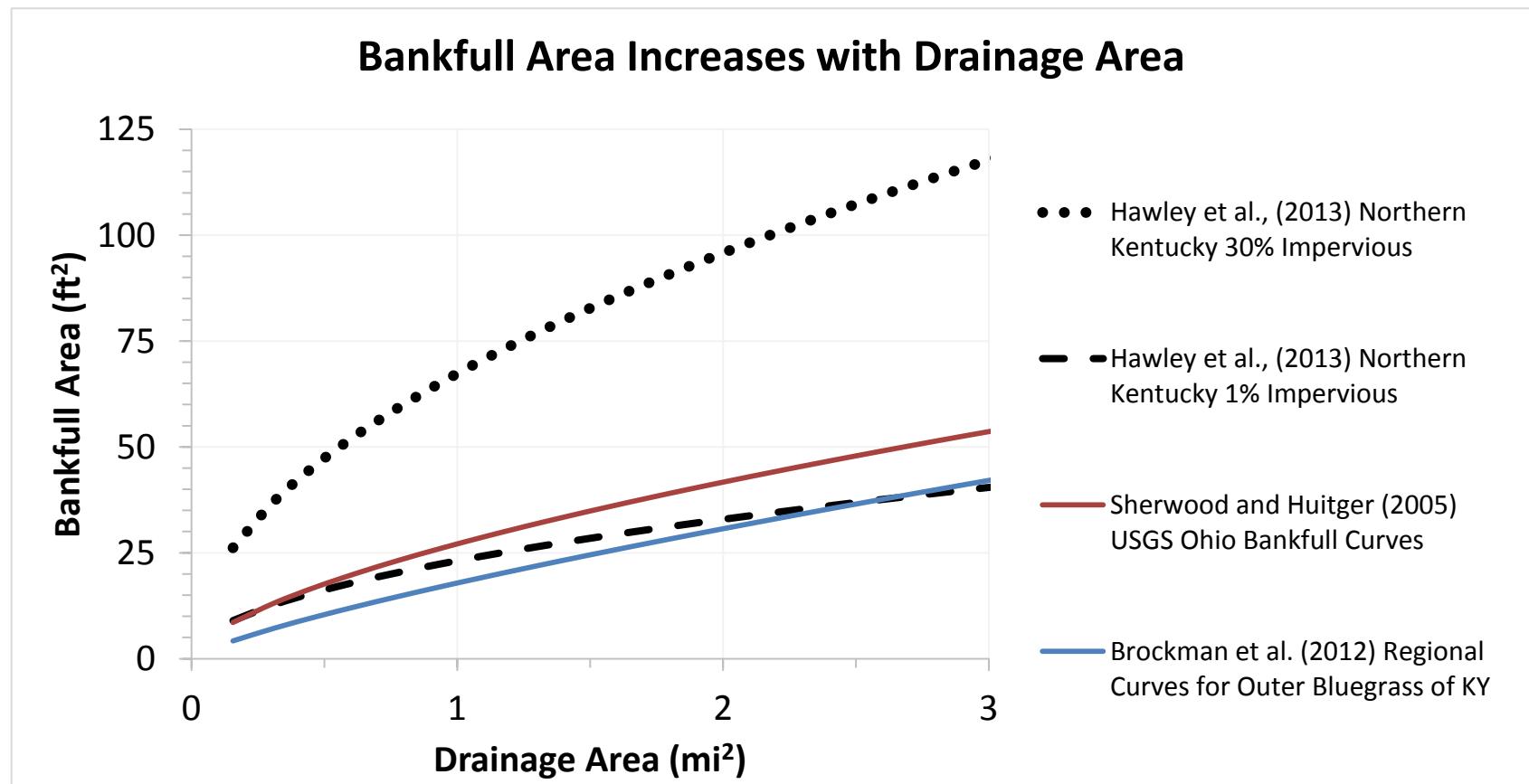


0.3" in 1 hour

06/10/2009 08:26

More Water = Larger Channels

More Storm Water = Larger Urban Streams



Adapted from Smith et al. (Forthcoming, Freshwater Science)

Reach Scale Stream Restoration



Biological

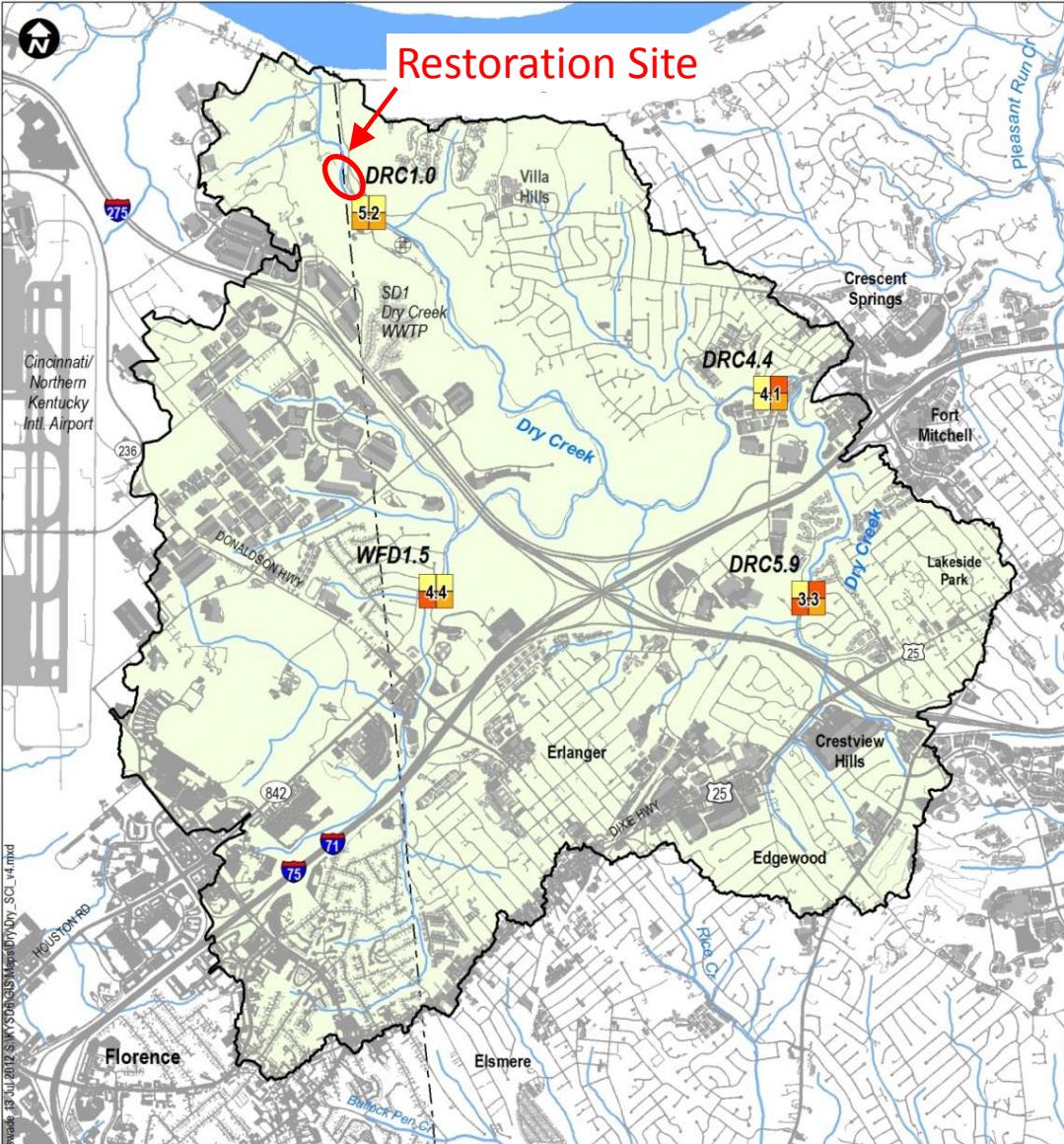
Water Quality

Physical/Habitat

Stream Flow

Land Use and Management





Reach Scale Projects Typically Show Limited Biological Improvement

Freshwater Biology (2009), 55 (Suppl. 1), 1–18

doi:10.1111/j.1365-2427.2009.02372.x

River restoration, habitat heterogeneity and biodiversity: a failure of theory or practice?

MARGARET A. PALMER^{*†}, HOLLY L. MENNINGER[‡] AND EMILY BERNHARDT[§]

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[†]*Department of Entomology, University of Maryland, College Park, MD, U.S.A.*

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[§]*Department of Biology, Duke University, Durham, NC, U.S.A.*

2 out of 78 projects (2.5%) showed significant increases in biodiversity

The Urban Flow Regime is often suspected for the Lack of Biological Success

INVITED FEATURE

Ecological Applications
Vol. 21, No. 6

Ecological Applications, 21(6), 2011, pp. 1932–1949
© 2011 by the Ecological Society of America

Effects of urbanization and urban stream restoration on the physical and biological structure of stream ecosystems

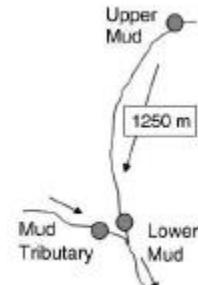
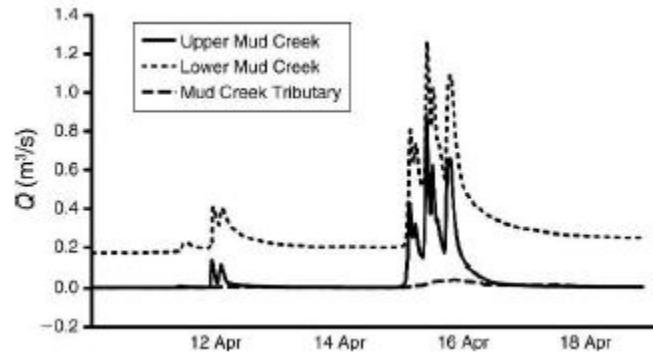
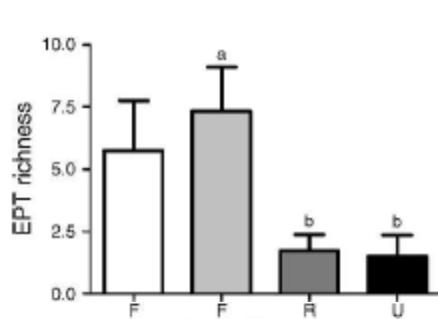
CHRISTY R. VIOLIN,^{1,5} PETER CADÀ,^{2,6} ELIZABETH B. SUDDUTH,³ BROOKE A. HASSETT,³ DAVID L. PENROSE,⁴ AND EMILY S. BERNHARDT³

¹Department of Biology, University of North Carolina, Chapel Hill, North Carolina 27599 USA

Nicholas School of the Environment, Duke University, Durham, North Carolina 27708 USA

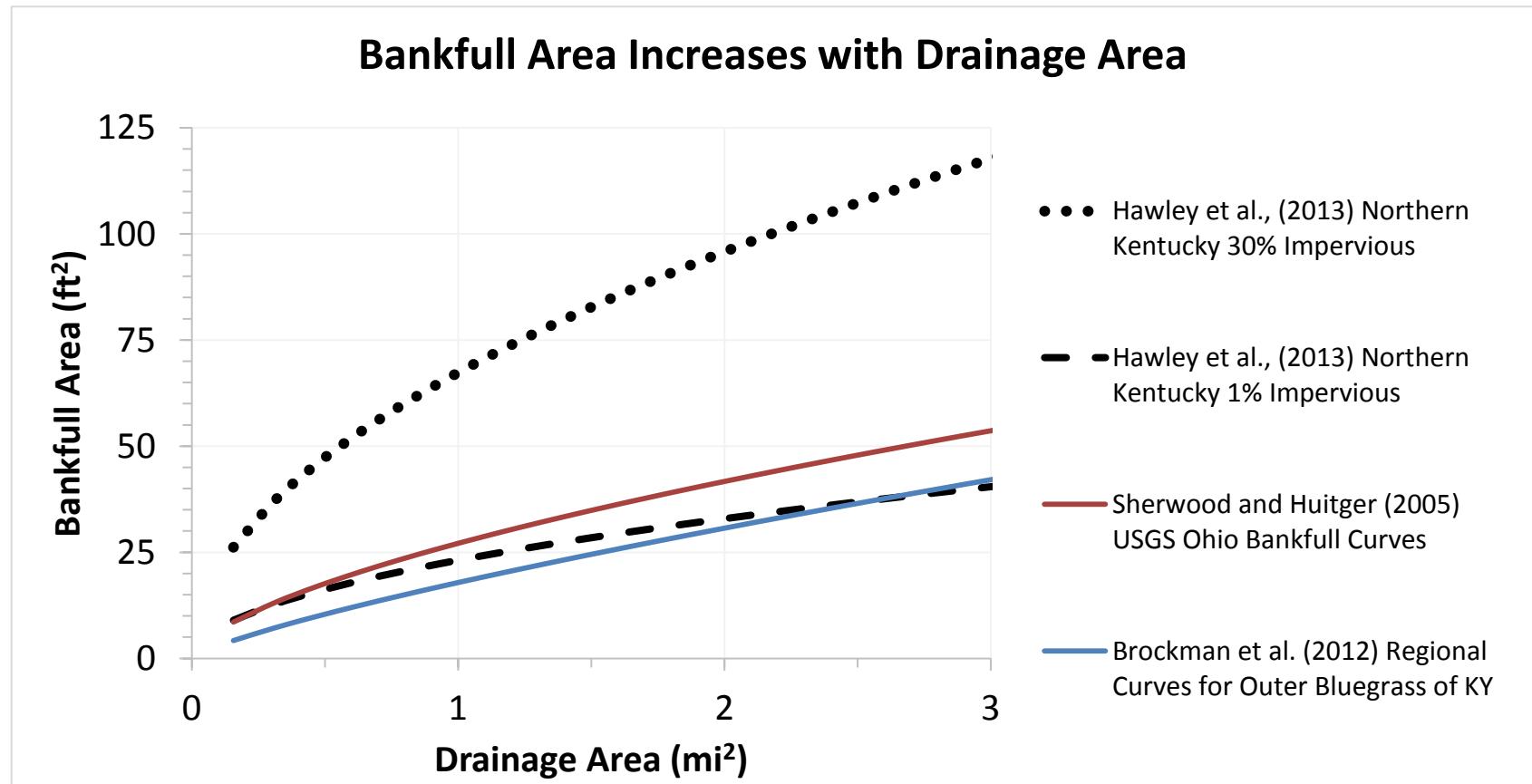
³Department of Biology, Duke University, Durham, North Carolina 27708 USA

⁴Department of Biological and Agricultural Engineering, North Carolina State University, Raleigh, North Carolina 27695 USA



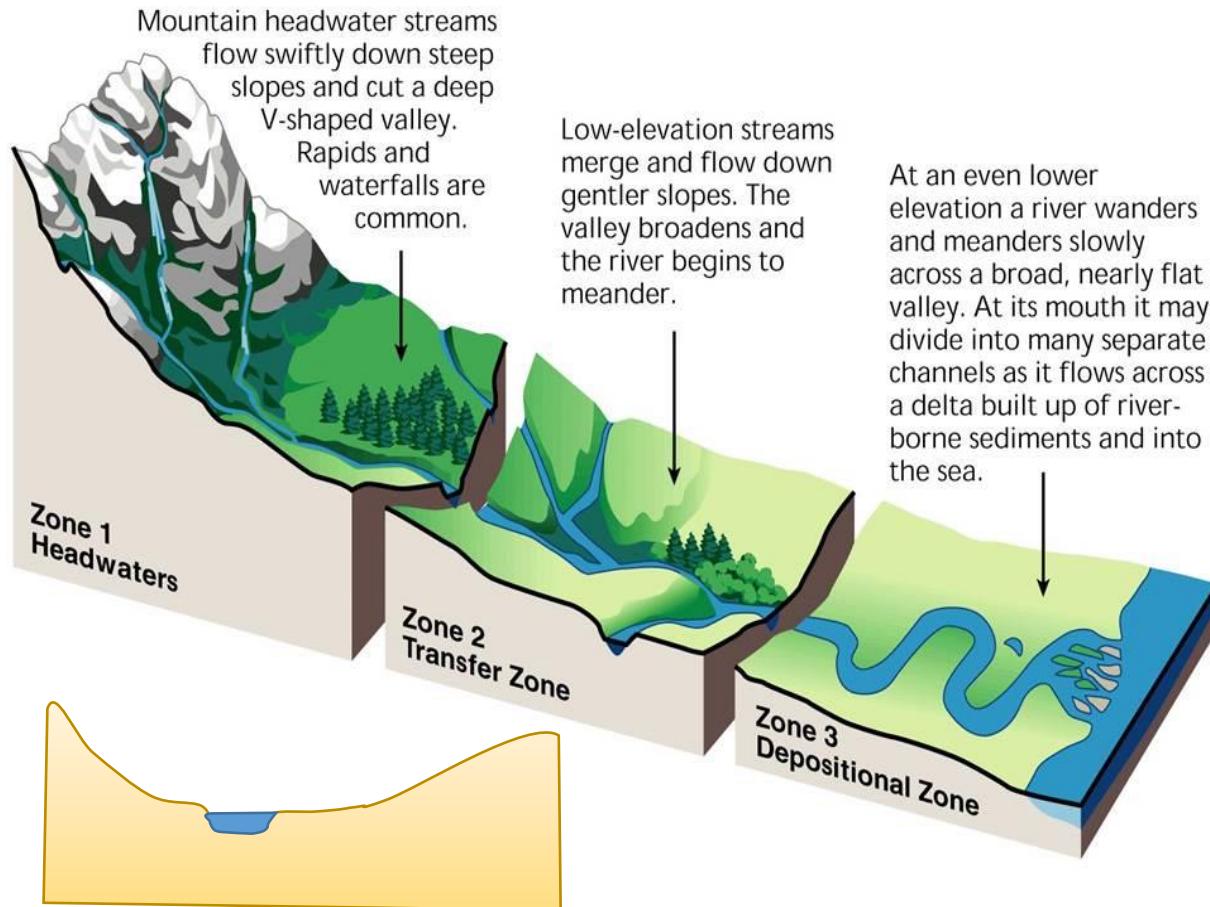
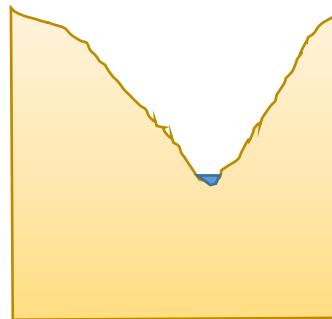
More Water = Larger Channels

More Stormwater = Larger Urban Streams

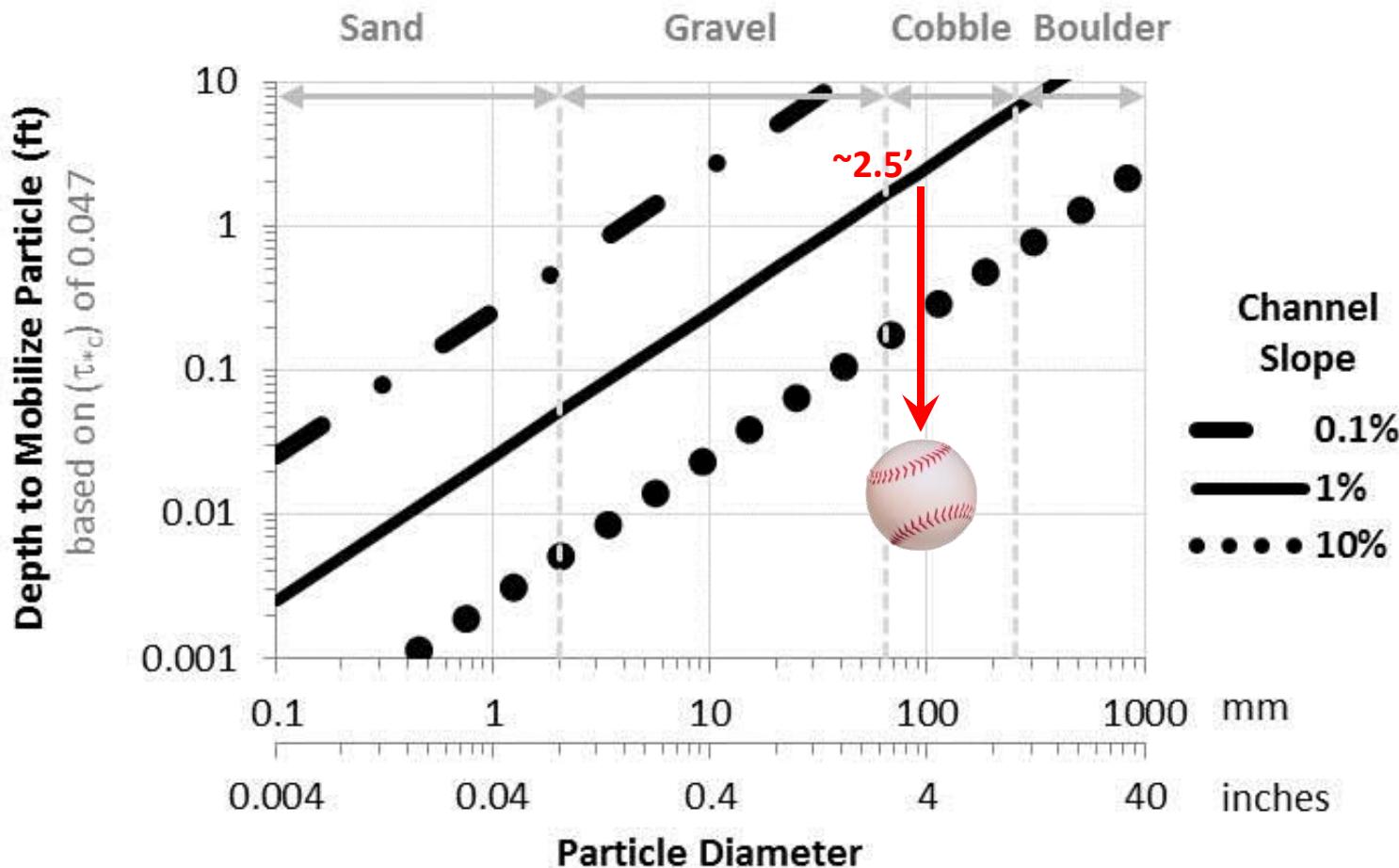


Adapted from Smith et al. (Forthcoming, Freshwater Science)

$Q_{critical}$ Also Depends on Channel & Valley Form

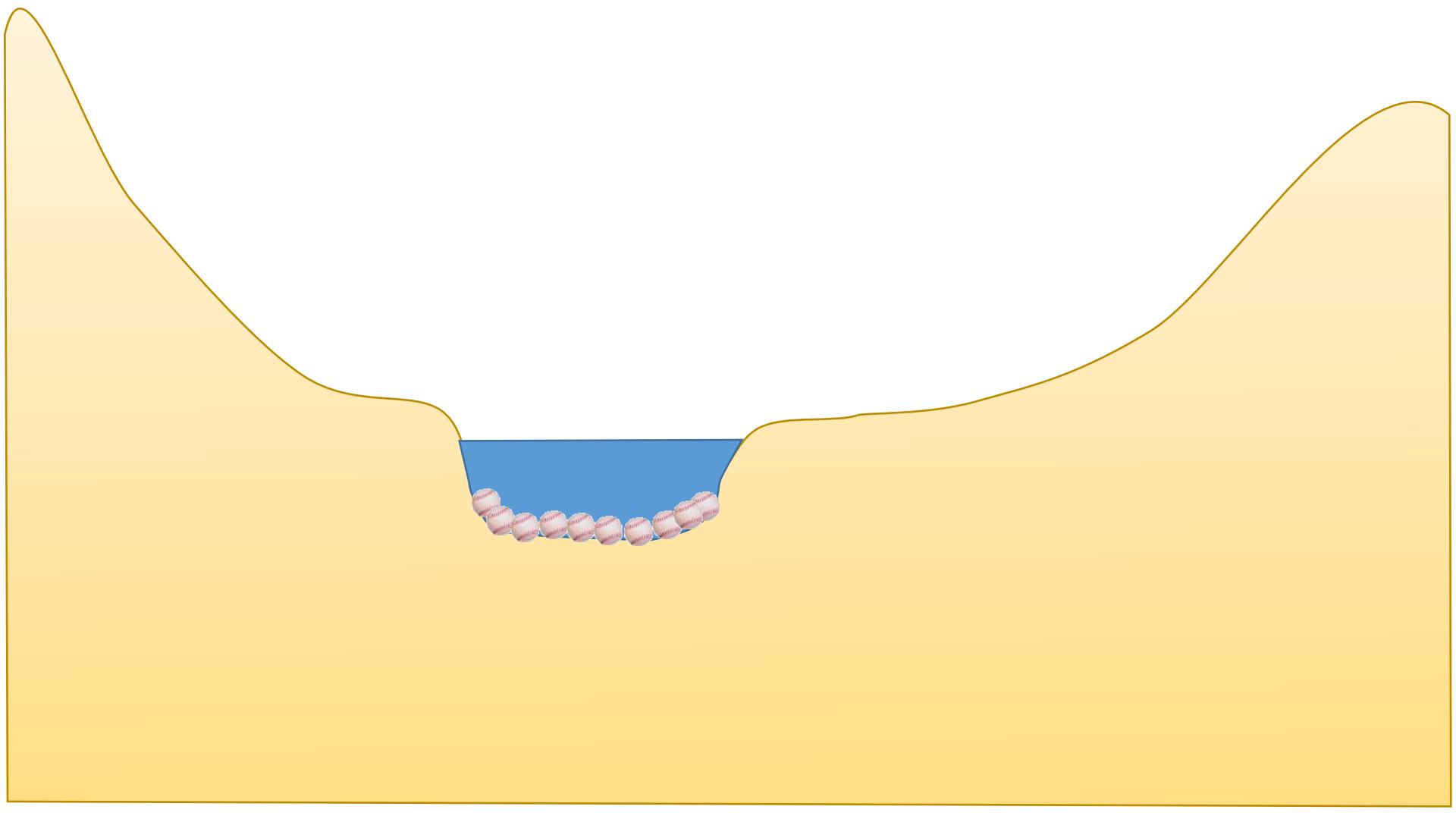


Softball Example: On 1% Slope, Required Depth to Mobilize Is 2.5'



Adapted from Hawley and Vietz (Forthcoming, Freshwater Science)

Softball Example: If Water Depth > 2.5' Bed Erosion Occurs



Softball Example: If Water Depth > 2.5' Bed Erosion Occurs

Relatively Poor Floodplain Connection
Channel Erosion



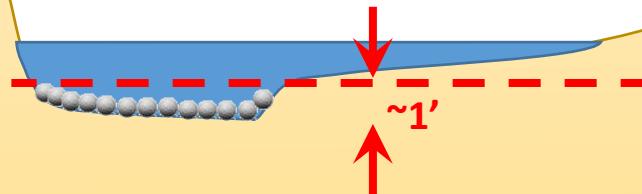
Softball Example: If Water Depth > 2.5' Bed Erosion Occurs

Relatively Good Floodplain Connection
No Channel Erosion

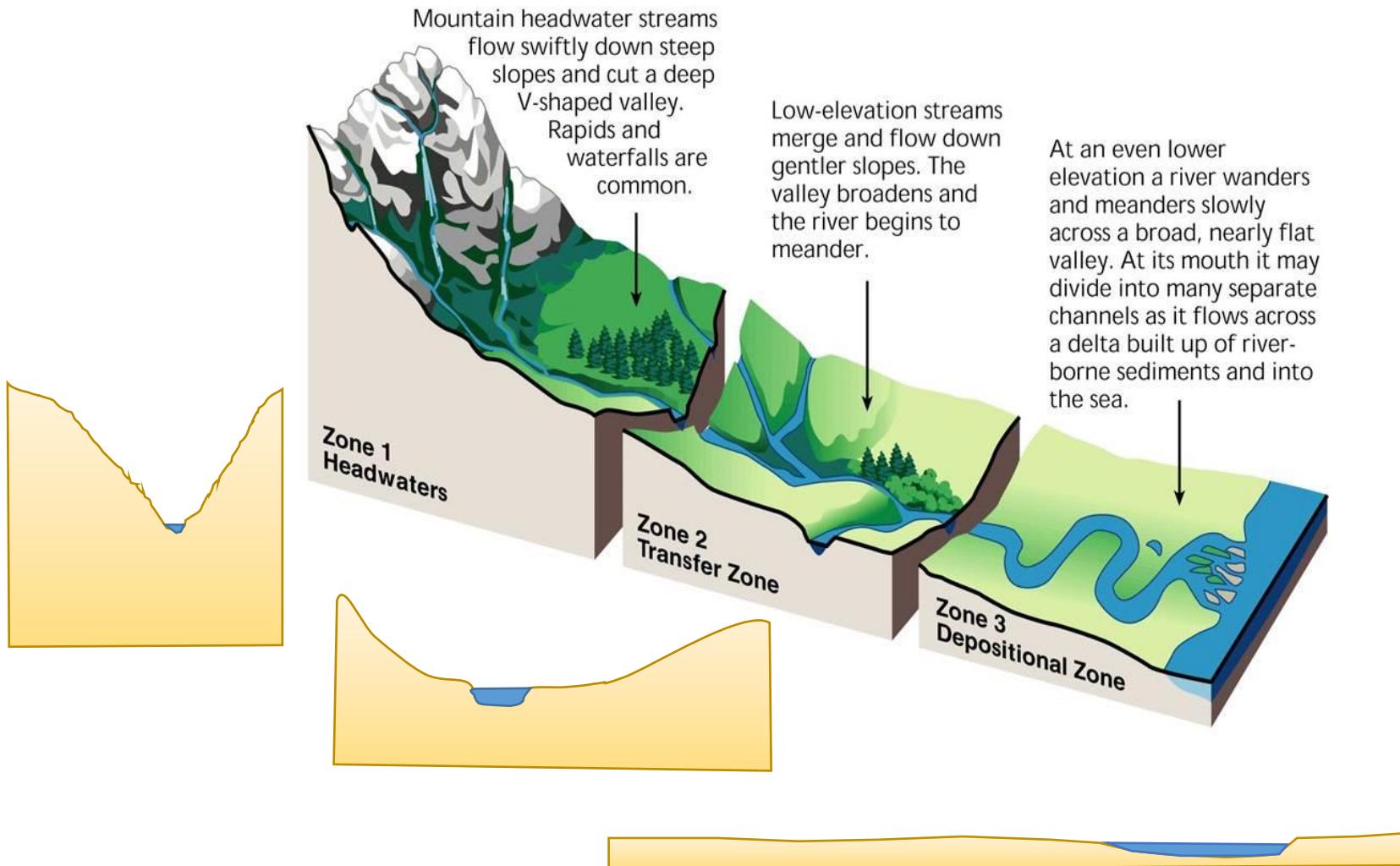


Golf Ball Example: On 1% Slope, Required Depth to Mobilize Is 1'

Relatively Good Floodplain Connection
Channel Erosion Still Occurs



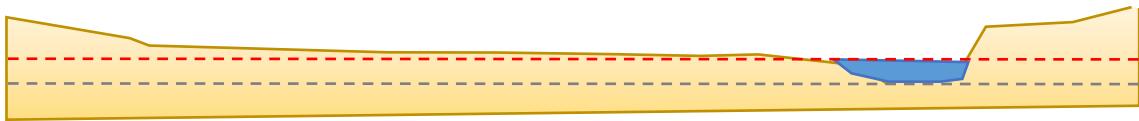
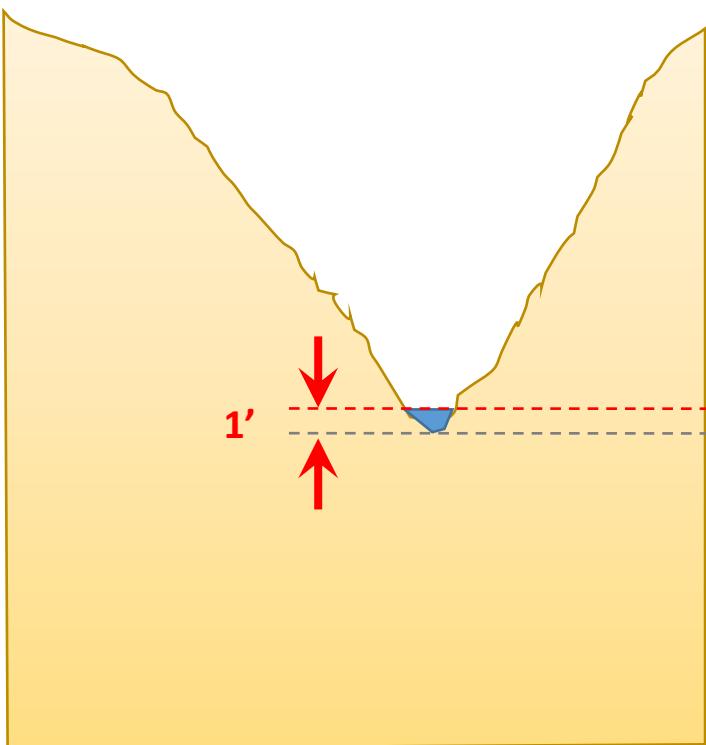
Floodplain Connectivity also Affects How Erosive A Flow Can Be



Confined vs. Unconfined Example: Low Flow

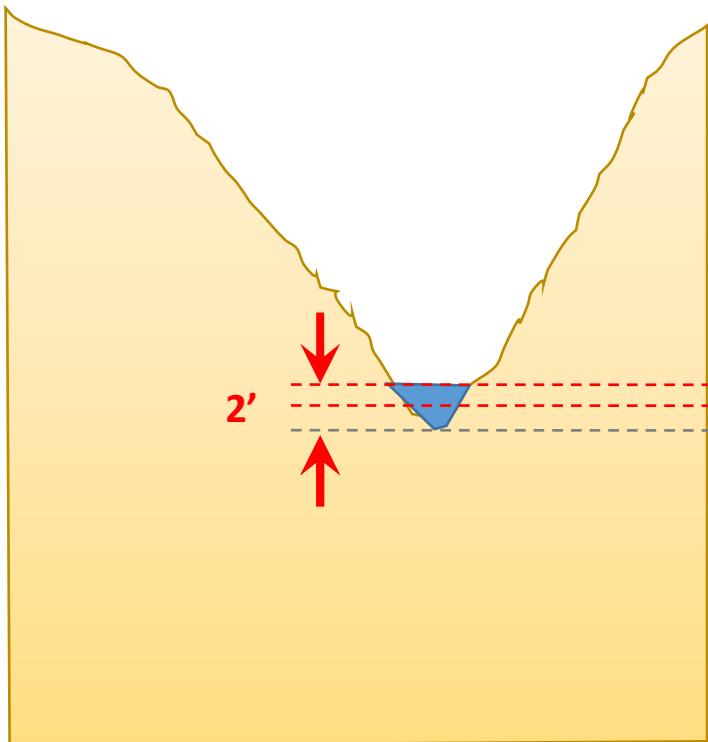
Confined Valley

*Unconfined Valley with
Well-Connected Floodplain*

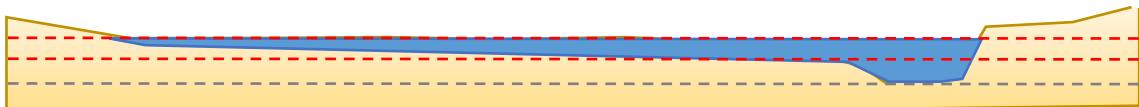


Confined vs. Unconfined Example: 1' Increase in Depth

Confined Valley
Small increase in flow

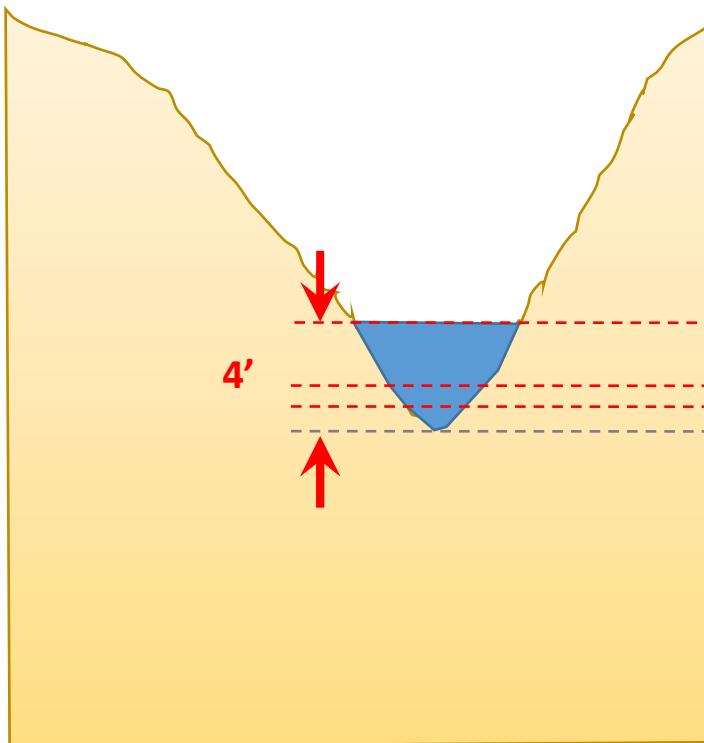


*Unconfined Valley with
Well-Connected Floodplain*
Large increase in flow



Confined vs. Unconfined Example: Required Depth to Convey Same Flow On Same Slope

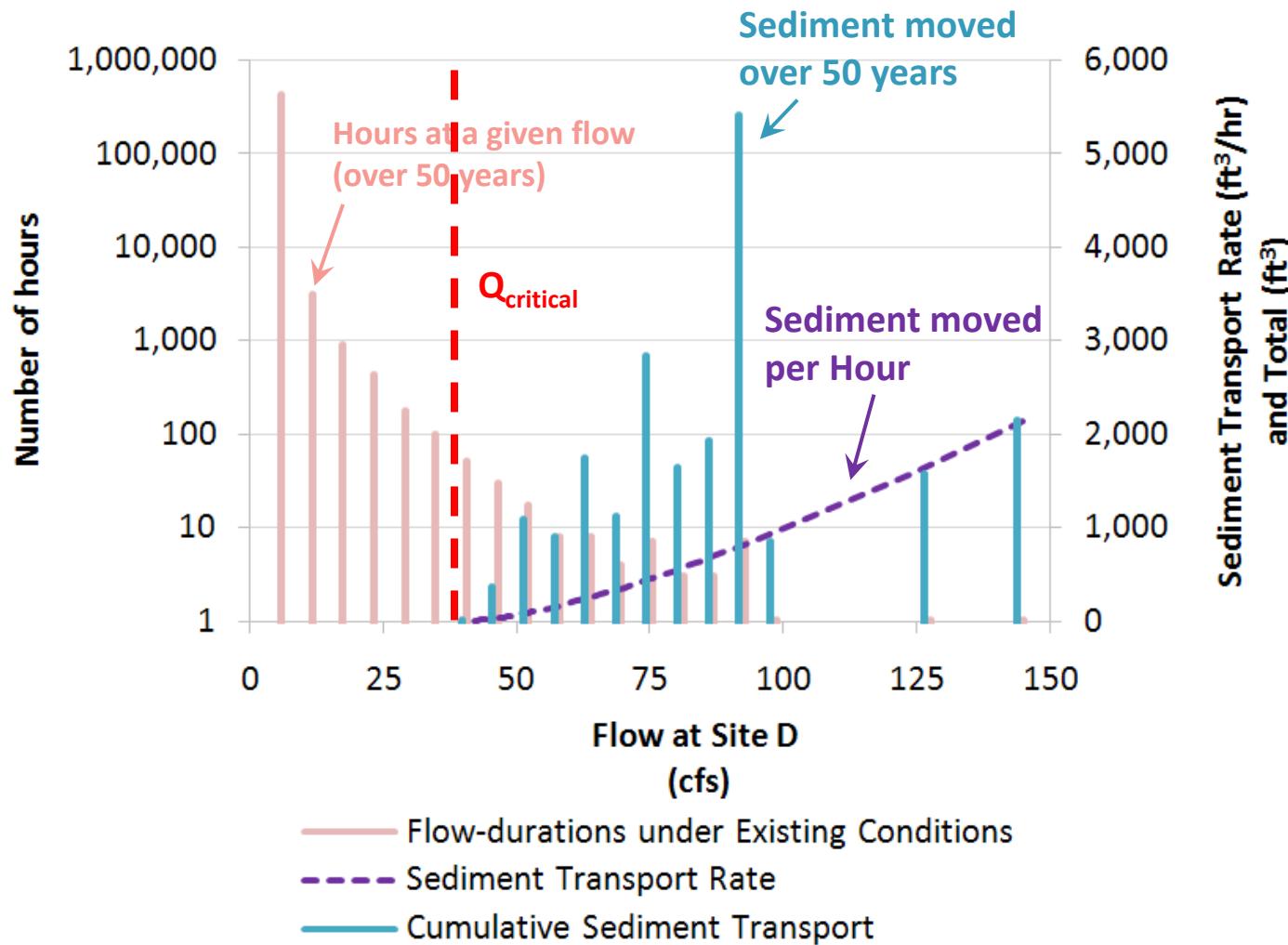
Confined Valley
4x low flow depth



*Unconfined Valley with
Well-Connected Floodplain*
2x low flow depth

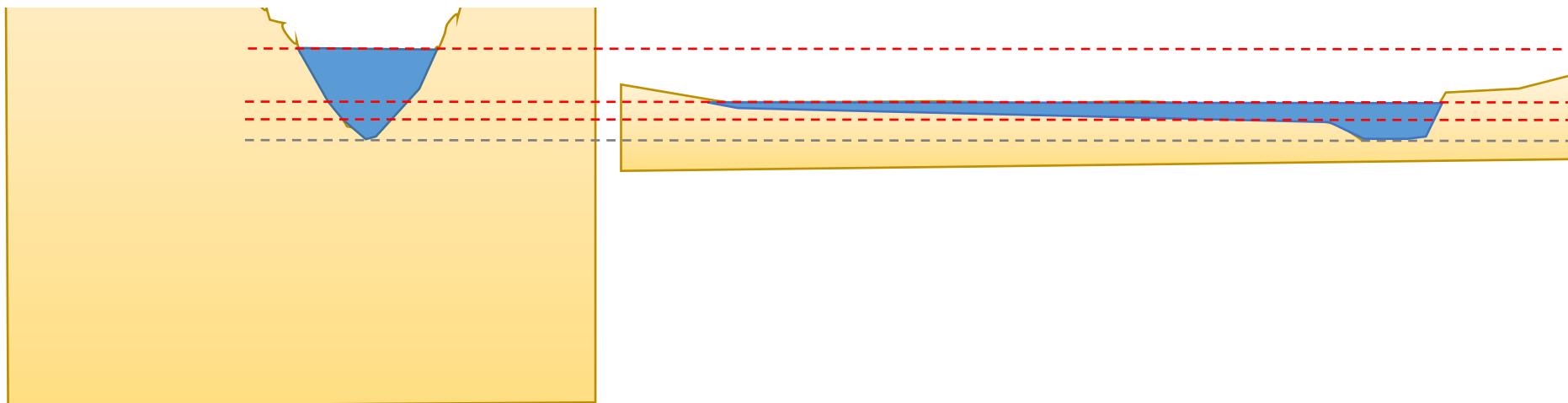
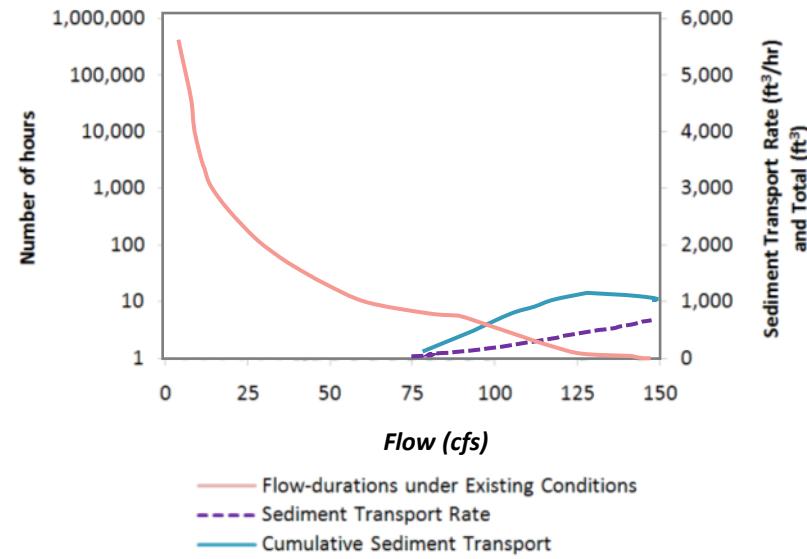
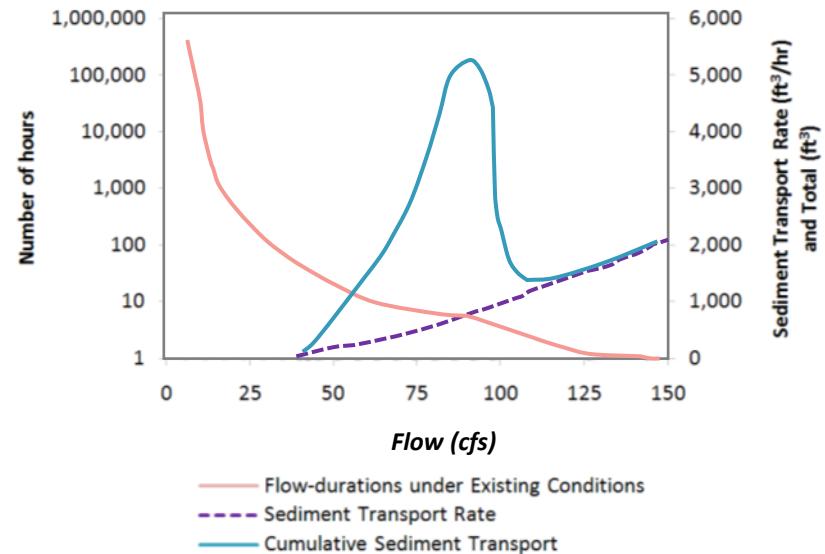


Above $Q_{critical}$, Sediment Transport Continues to Increase with Deeper Flows



Adapted from Hawley et al. (2012)

Confined vs. Unconfined Example: Sediment Transport Potential

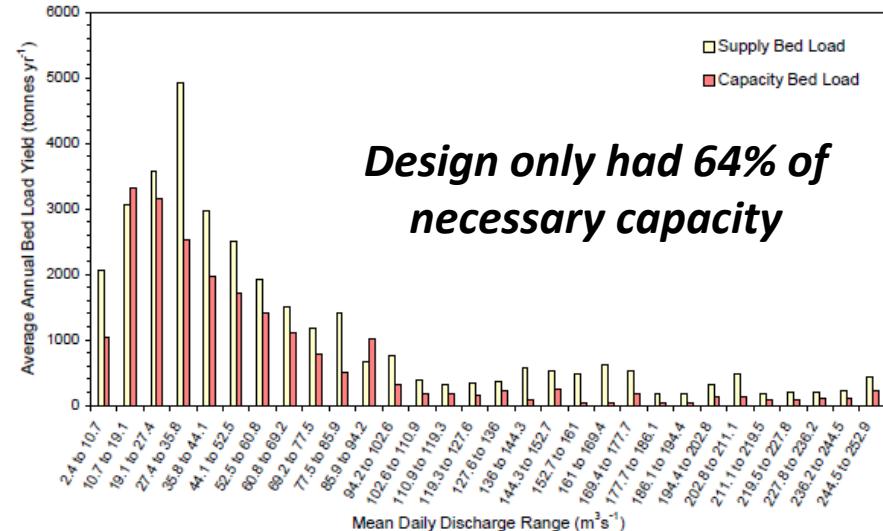


Matching Long-term Sediment Transport Is Critical For Geomorphic Equilibrium

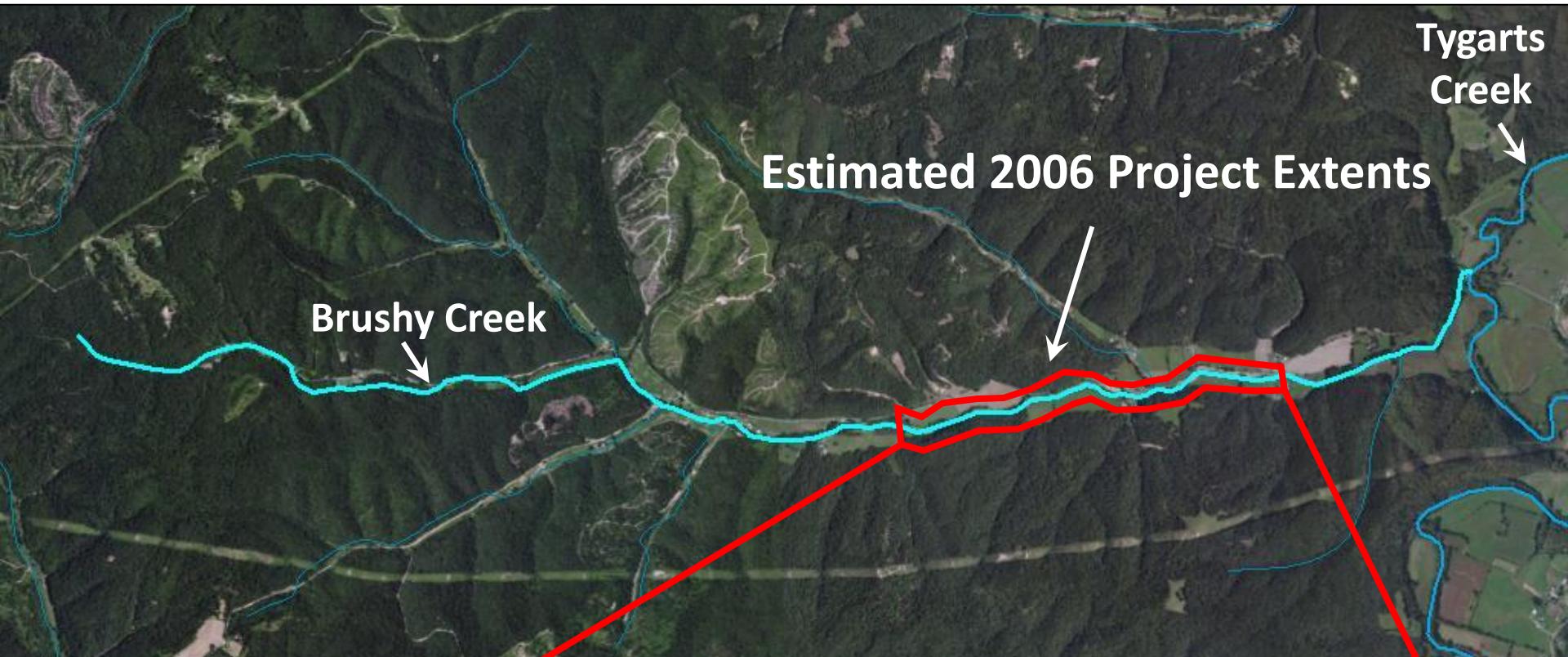


Soar & Thorne, 2001

- Insufficient transport capacity
→ Aggradation



Similar Failures Evident with Regional Projects



Similar Failures Evident with Regional Projects

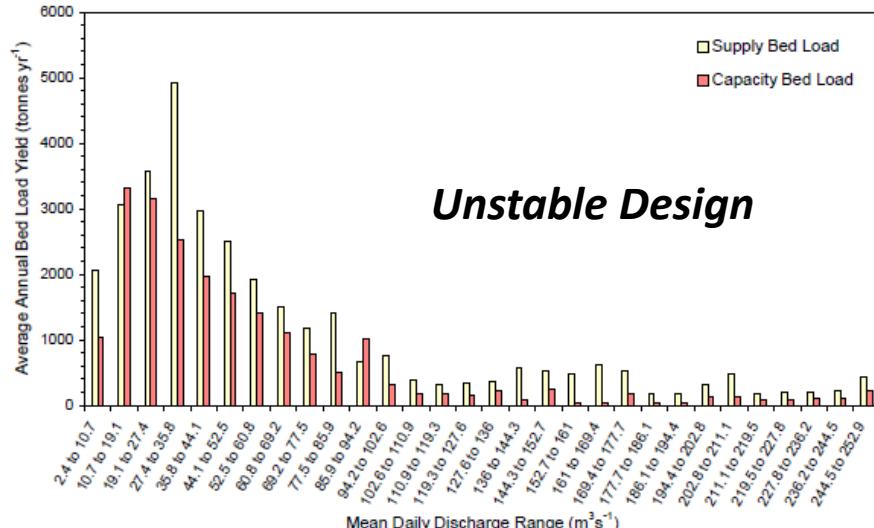
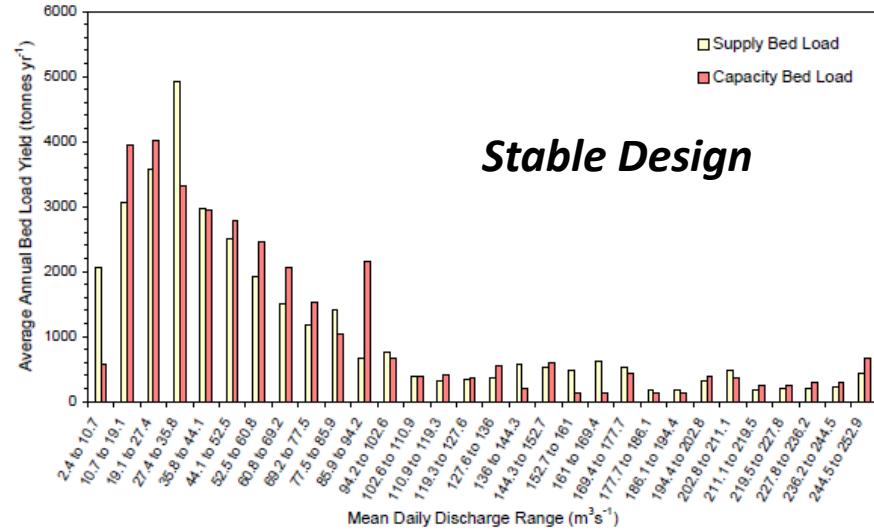


Similar Failures Evident with Regional Projects

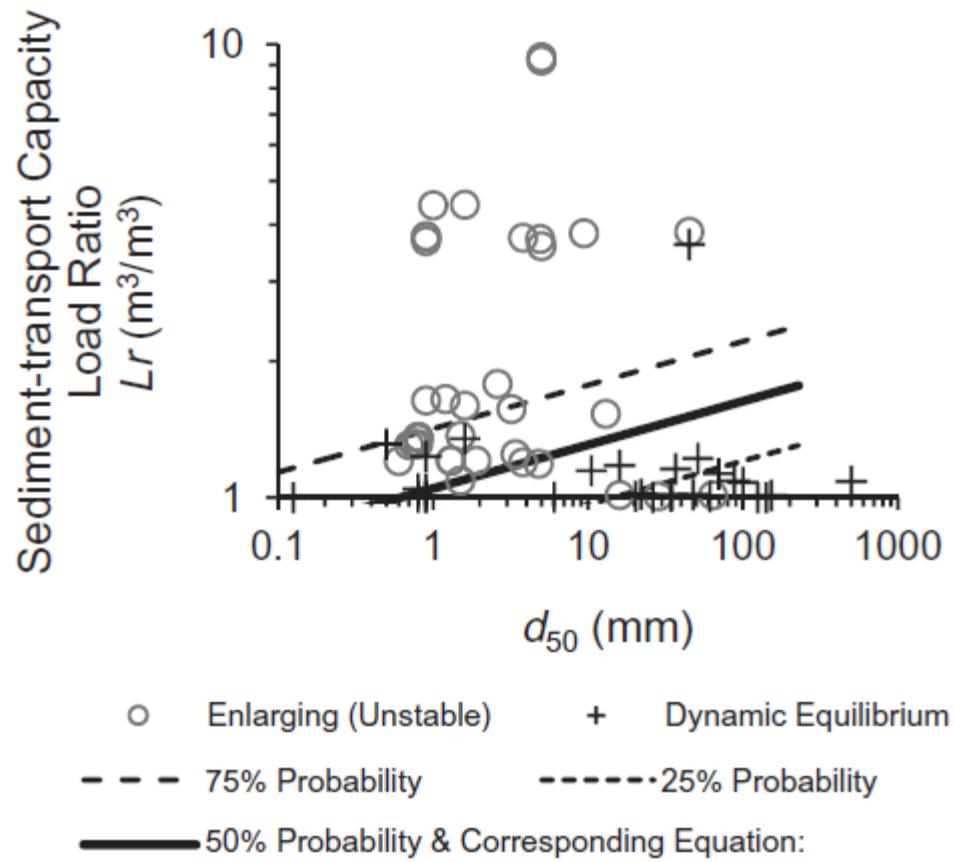
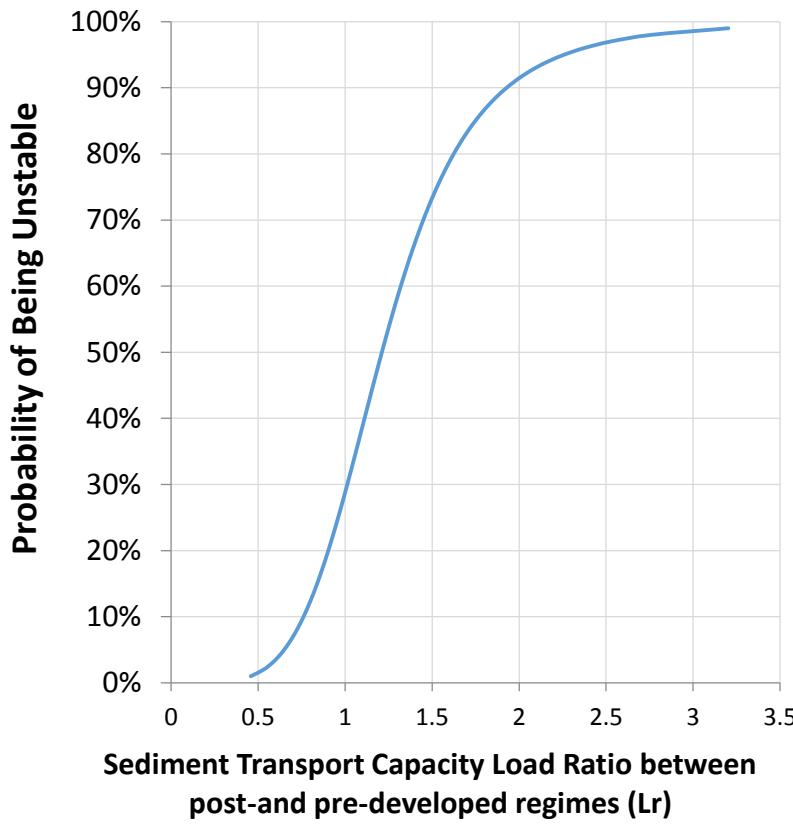


Sediment Transport Continuity Should Be A Critical Design Factor

- Stream Restoration
- Stormwater Management



Stormwater Designs that Fail to Match Pre-developed Sediment Loads → Stream Instability



$$L_r = 1.04 * d_{50}^{0.120}$$

Adapted from Hawley and Bledsoe (2013)